

MECHANICAL FAILURE

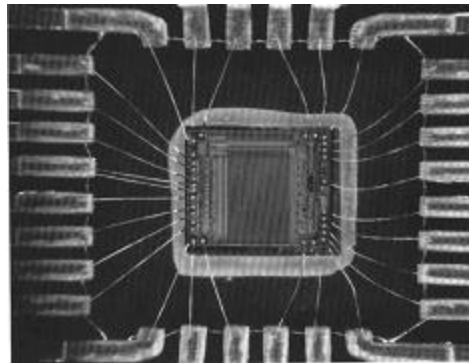
Mechanical Failure

ISSUES TO ADDRESS...

- How do flaws in a material initiate failure?
- How is fracture resistance quantified; how do different material classes compare?
- How do we estimate the stress to fracture?
- How do loading rate, loading history, and temperature affect the failure stress?



Ship-cyclic loading
from waves.



Computer chip-cyclic
thermal loading.



Hip implant-cyclic
loading from walking.

What is a Fracture?

- **Fracture** is the separation of a body into two or more pieces in response to an imposed stress.
- The applied stress may be *tensile, compressive, shear, or torsional.*
- Stress can be caused by forces, temperature, etc.
- Any fracture process involves two steps—**crack formation** and **propagation**—in response to an imposed stress.

Fracture Modes

- **Ductile fracture**

- Occurs with plastic deformation
- **Material absorbs energy before fracture**
- Crack is called stable crack: crack growth occurs with plastic deformation . Also, increasing stress is required for crack propagation.

- **Brittle fracture**

- Little or no plastic deformation
- **Material absorb low energy before fracture**
- Crack is called unstable crack.
- Catastrophic fracture (sudden)

Ductile vs Brittle Failure

- **Classification:**

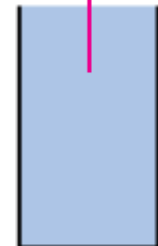
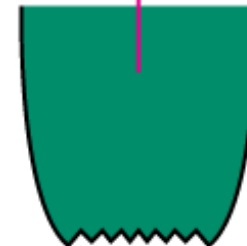
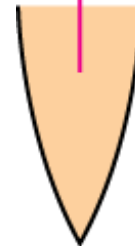
**Fracture
behavior:**

**Very
Ductile**

**Moderately
Ductile**

Brittle

$(\%EL)=100\%$



Large

Moderate

Small

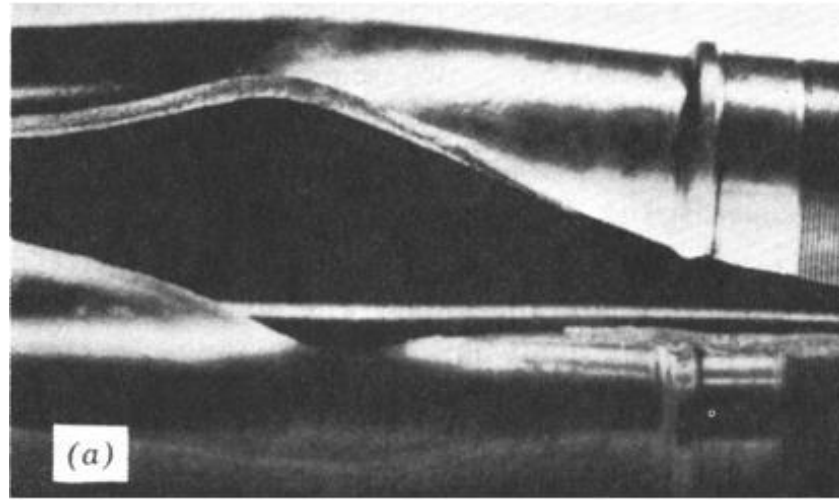
- **Ductile fracture is usually desirable!**

Ductile:
warning before fracture, as increasing force is required for crack growth

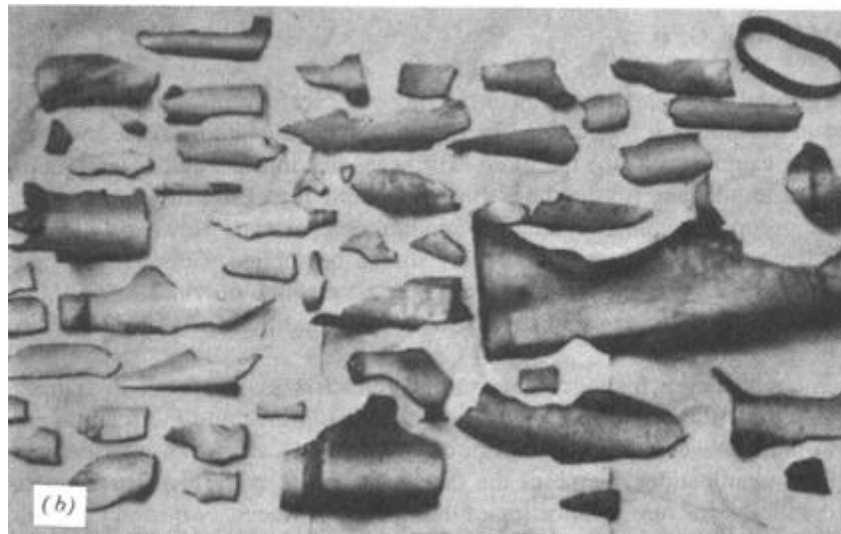
Brittle:
No warning

Example: Failure of a Pipe

- **Ductile failure:**
 - one/two piece(s)
 - large deformation

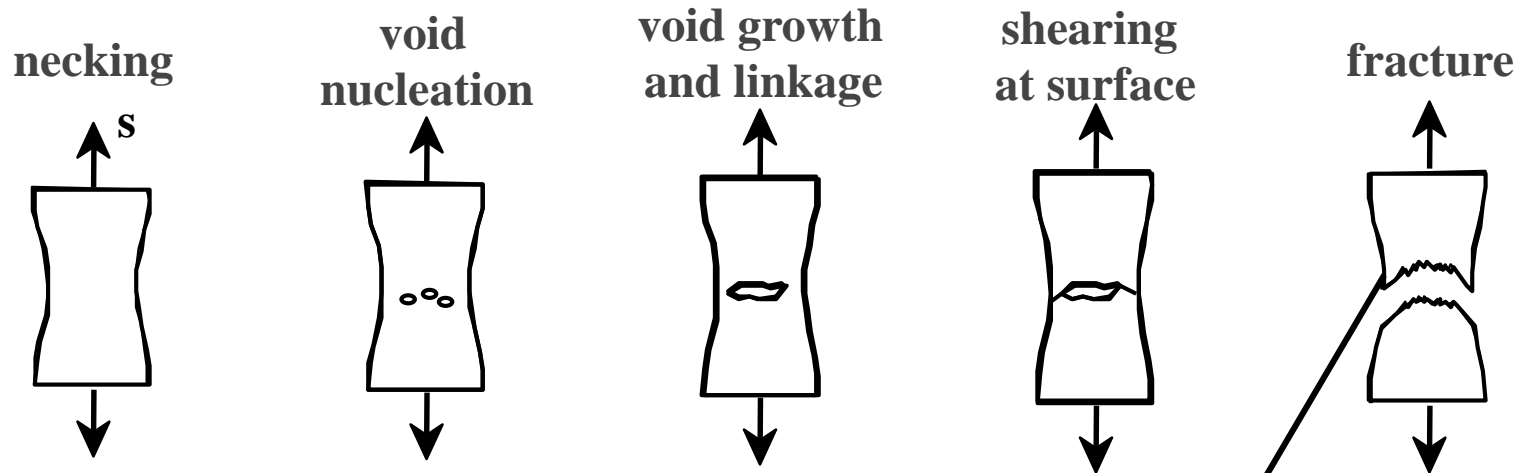


- **Brittle failure:**
 - many pieces
 - small deformation

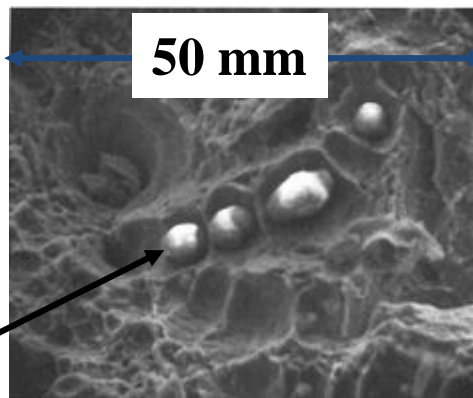


Moderately Ductile Failure- Cup & Cone Fracture

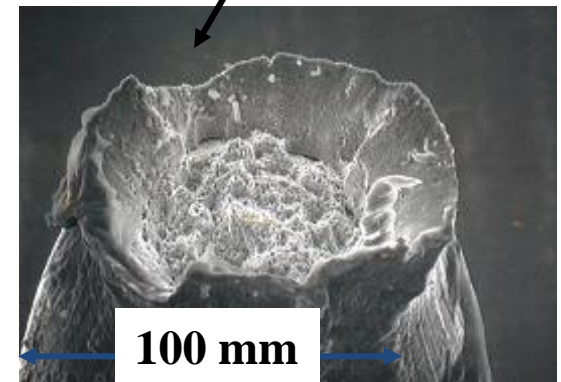
- Evolution to failure:



- Resulting fracture surfaces (steel)



particles serve as void nucleation sites.



crack occurs perpendicular to tensile force applied

Ductile vs. Brittle Failure

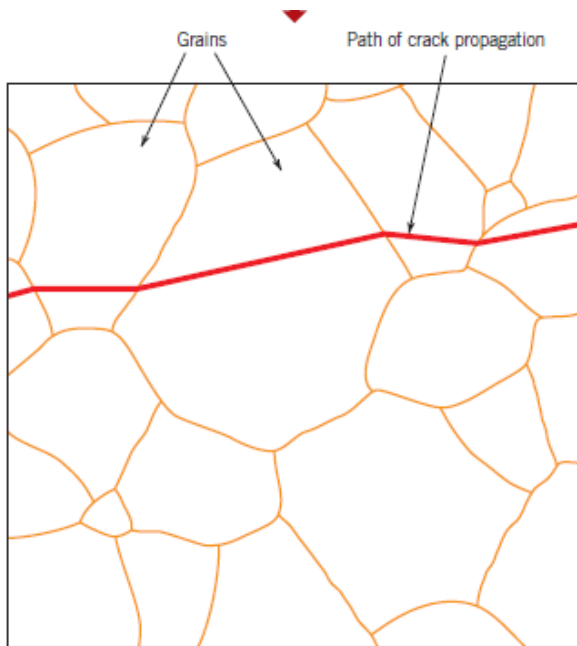


cup-and-cone fracture

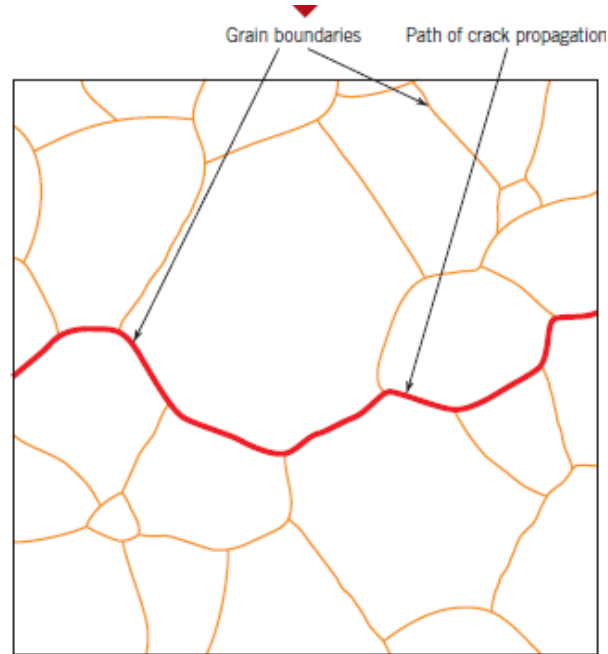


brittle fracture

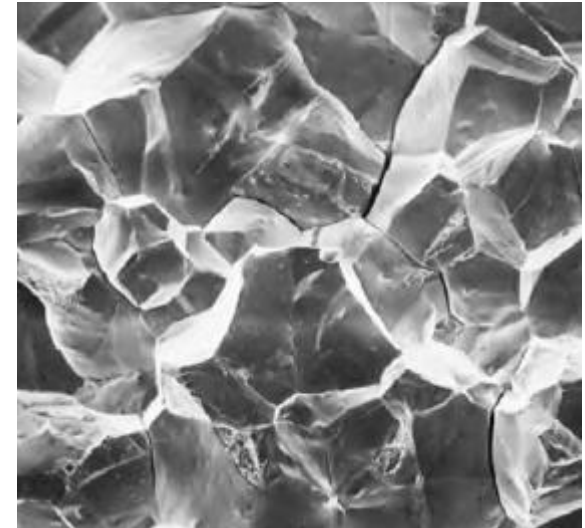
Transgranular vs Intergranular Fracture



**Trans-granular
Fracture**



Intergranular Fracture

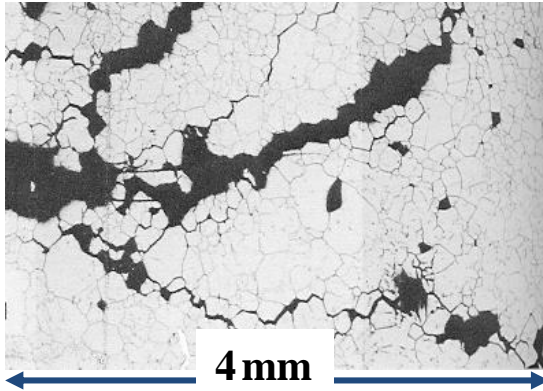


Brittle Fracture

Brittle Fracture Surfaces

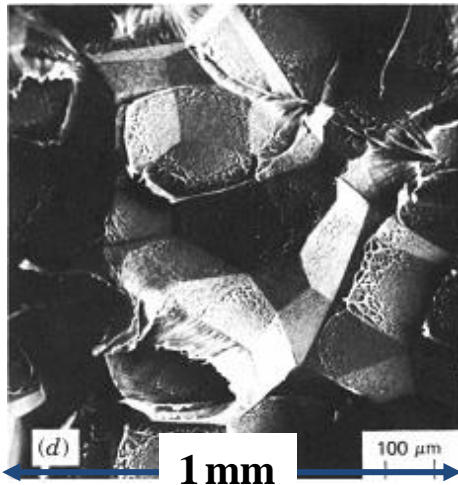
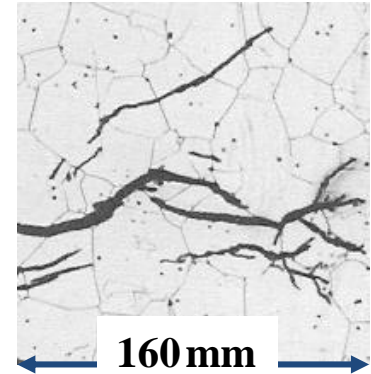
- Intergranular
(between grains)

304 S. Steel
(metal)



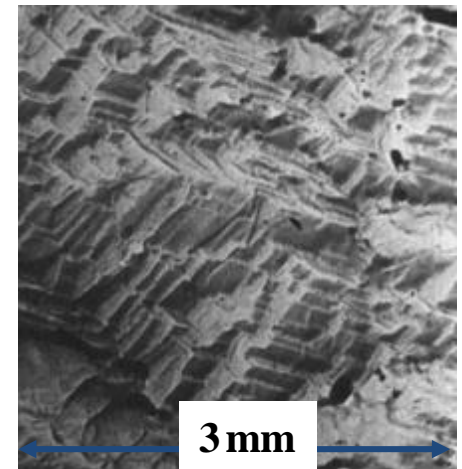
- Transgranular
(within grains)

316 S. Steel
(metal)



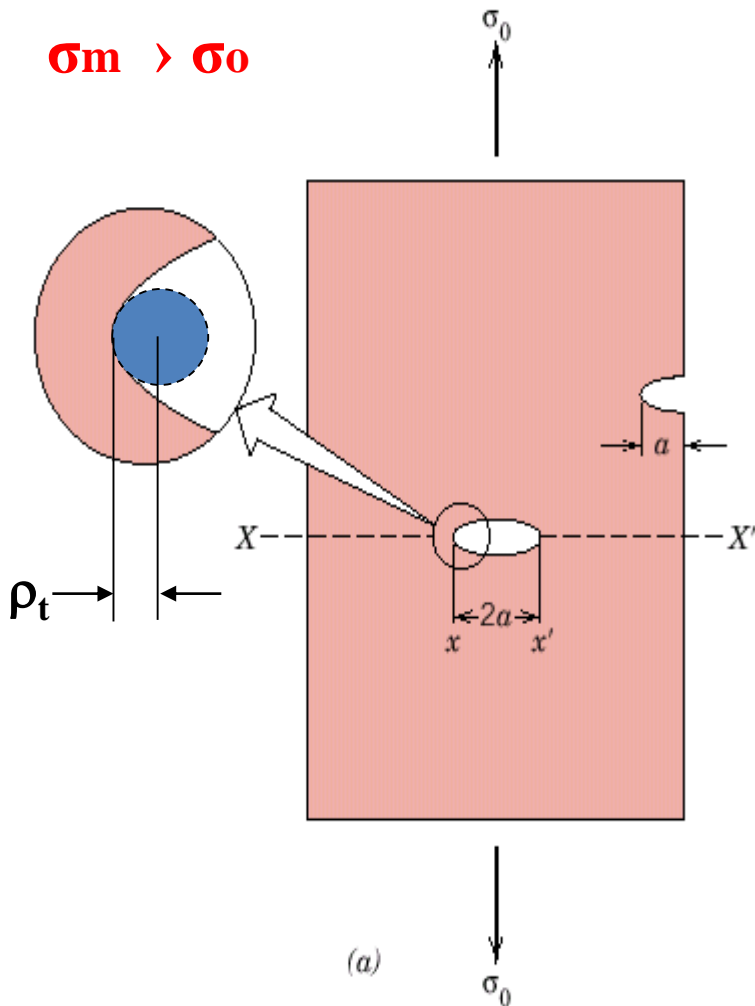
Polypropylene
(polymer)

Al Oxide
(ceramic)



Stress Concentration- Stress Raisers

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Suppose an internal flaw (crack) already exists in a material and it is assumed to have a shape like a elliptical hole:

The maximum stress (σ_m) occurs at crack tip:

$$\sigma_m = 2\sigma_o \left(\frac{a}{\rho_t} \right)^{1/2} = K_t \sigma_o$$

where

ρ_t = radius of curvature at crack tip

σ_o = applied stress

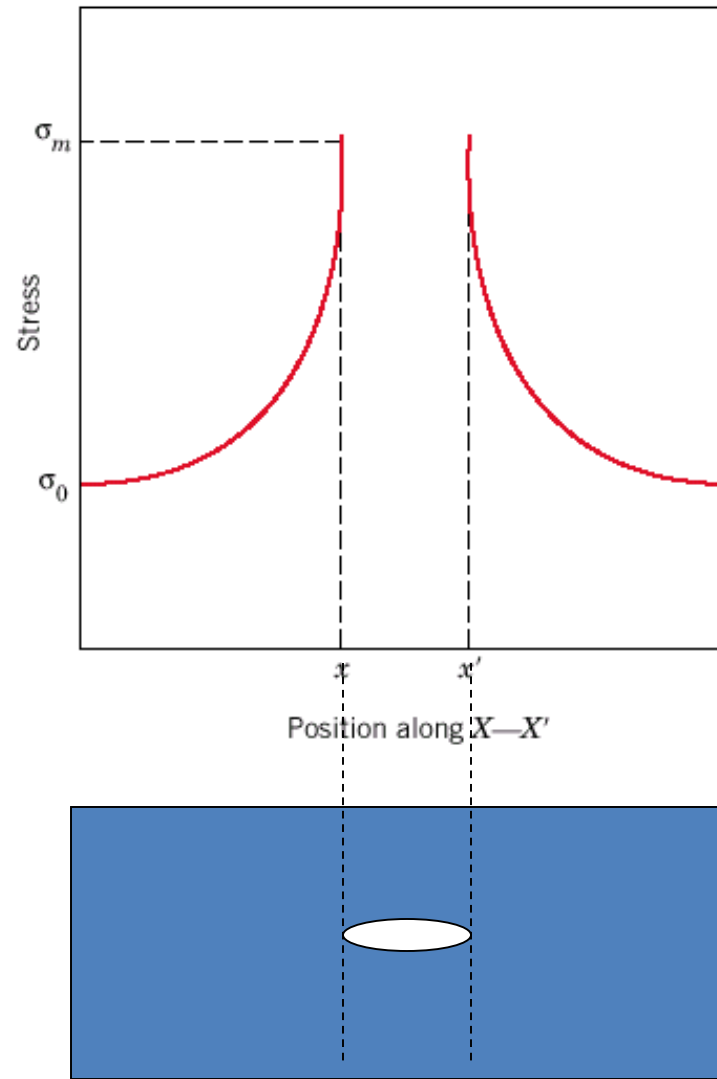
σ_m = stress at crack tip

K_t = Stress concentration factor

Theoretical fracture strength is higher than practical one; *Why?*

Concentration of Stress at Crack Tip

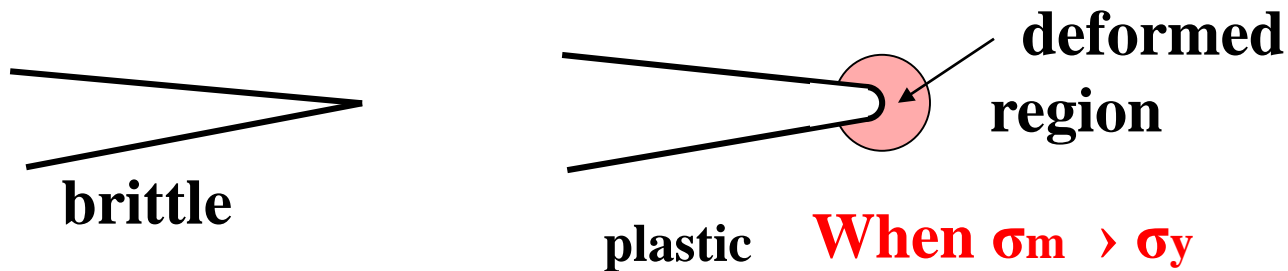
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Crack Propagation

Cracks propagate due to sharpness of crack tip

- A plastic material deforms at the tip, “blunting” the crack.



Effect of **stress raiser** is more significant in brittle materials than in ductile materials. When σ_m exceeds σ_y , plastic deformation of metal in the region of crack occurs thus blunting crack. However, in brittle material, it does not happen.

When Does a Crack Propagate?

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Crack propagation in a **brittle** material occurs if

$$\sigma_m > \sigma_c$$

$$\sigma_c = \left(\frac{2E\gamma_s}{\pi a} \right)^{1/2}$$

$$\sigma_m = 2\sigma_o \left(\frac{a}{\rho_t} \right)^{1/2} = K_t \sigma_o$$

Where

- σ_c = Critical stress to propagate crack
- E = modulus of elasticity
- γ_s = specific surface energy (J/m²)
- a = one half length of internal crack

For ductile => replace γ_s by $\gamma_s + \gamma_p$

where γ_p is plastic deformation energy

Example – Brittle Fracture

- Given Glass Sheet with
 - Tensile Stress,
 $\sigma = 40 \text{ Mpa}$
 - $E = 69 \text{ GPa}$
 - $\gamma = 0.3 \text{ J/m}$
- Find Maximum Length of a Surface Flaw
- Plan

- Set $\sigma_c = 40 \text{ Mpa}$
- Solve Griffith Eqn for Edge-Crack Length

$$a = \frac{2E\gamma_s}{\pi\sigma_{applied}^2}$$

■ Solving

$$a = \frac{2(69 \times 10^9 \text{ N/m}^2)(0.3 \text{ N/m})}{\pi(40 \times 10^6 \text{ N/m}^2)^2}$$

$$a = 8.2 \times 10^{-6} \text{ m} = 8.2 \mu\text{m}$$

Fracture Toughness: Design Against Crack Growth

- Crack growth condition:

$$K_c = Y \sigma_c \sqrt{\pi a}$$

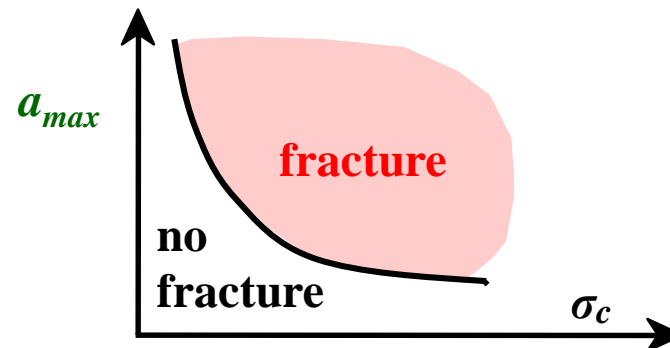
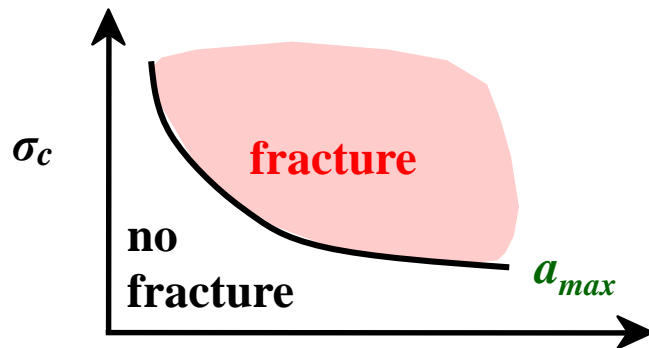
- Largest**, most **stressed** cracks grow first!

--**Result 1**: Max. flaw size dictates design stress (max allowable stress).

$$\sigma_{design} < \frac{K_c}{Y \sqrt{\pi a_{max}}}$$

--**Result 2**: Design stress dictates max. allowable flaw size.

$$a_{max} < \frac{1}{\pi} \left(\frac{K_c}{Y \sigma_{design}} \right)^2$$



Design Example: Aircraft Wing

- Material has $K_{Ic} = 26 \text{ MPa}\cdot\text{m}^{0.5}$
- Two designs to consider...

Design A

- largest flaw is 9 mm
- failure stress = 112 MPa

Design B

- use same material
- largest flaw is 4 mm
- failure stress = ?

- Use...

$$\sigma_c = \frac{K_{Ic}}{Y\sqrt{\pi a_{\max}}}$$

- Key point: Y and K_{Ic} are the same for both designs.

$$\frac{K_{Ic}}{Y\sqrt{\pi}} = \sigma\sqrt{a} = \text{constant}$$

--Result:

$$\left(\overset{112 \text{ MPa}}{\sigma_c} \sqrt{\overset{9 \text{ mm}}{a_{\max}}} \right)_A = \left(\overset{4 \text{ mm}}{\sigma_c} \sqrt{a_{\max}} \right)_B$$

$$\text{Answer: } (\sigma_c)_B = 168 \text{ MPa}$$

Design using fracture mechanics

$$\sigma_c \leq \frac{K_{Ic}}{Y\sqrt{\pi a}}$$

$$a_c = \frac{1}{\pi} \left(\frac{K_{Ic}}{\sigma Y} \right)^2$$

Example:

Compare the critical flaw sizes in the following metals subjected to tensile stress 1500MPa and $K = 1.12 \sigma\sqrt{\pi a}$.

	<u>K_{Ic} (MPa.m^{1/2})</u>	<u>Critical flaw size (microns)</u>
Al	250	7000
Steel	50	280
Zirconia(ZrO ₂)	2	0.45
Toughened Zirconia	12	16

SOLUTION

$$a_c = \frac{1}{\pi} \left(\frac{K_{Ic}}{\sigma Y} \right)^2$$

Where $Y = 1.12$. Substitute values

8.14 A specimen of 4340 steel alloy with a plane strain fracture toughness of $54.8 \text{ MPa} \sqrt{\text{m}}$ ($50 \text{ ksi} \sqrt{\text{in.}}$) is exposed to a stress of 1030 MPa ($150,000 \text{ psi}$). Will this specimen experience fracture if it is known that the largest surface crack is 0.5 mm (0.02 in.) long? Why or why not? Assume that the parameter Y has a value of 1.0 .

This problem asks to determine whether or not the 4140 steel alloy specimen will fracture when exposed to a stress of 1000 MPa, given the values of K_{Ic} , Y , and the largest value of a in the material.

The required stress before fracture is given by equation (8.7). Thus

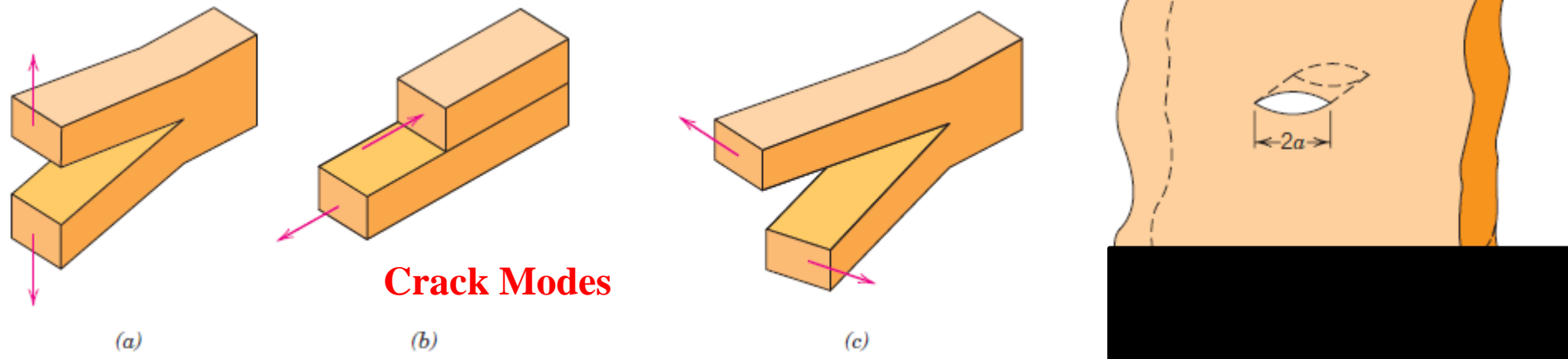
$$\sigma_c = \frac{K_{Ic}}{Y \sqrt{\pi a}} = \frac{54.8 \text{ MPa}\sqrt{\text{m}}}{(1) \sqrt{(\pi) (0.5 \times 10^{-3} \text{ m})}} = 1380 \text{ MPa} \quad (199,500 \text{ psi})$$

Therefore, fracture will not occur because this specimen will tolerate a stress of 1380 MPa (199,500 psi) before fracture, which is greater than the applied stress of 1000 MPa (150,000 psi).

Fracture Toughness

- For relatively thin specimens, the value of K_{Ic} will depend on specimen thickness. However, when specimen thickness is much greater than the crack dimensions, K_{Ic} becomes independent of thickness.
- The K_{Ic} value for this thick-specimen situation is known as the plane strain fracture toughness K_{Ic}

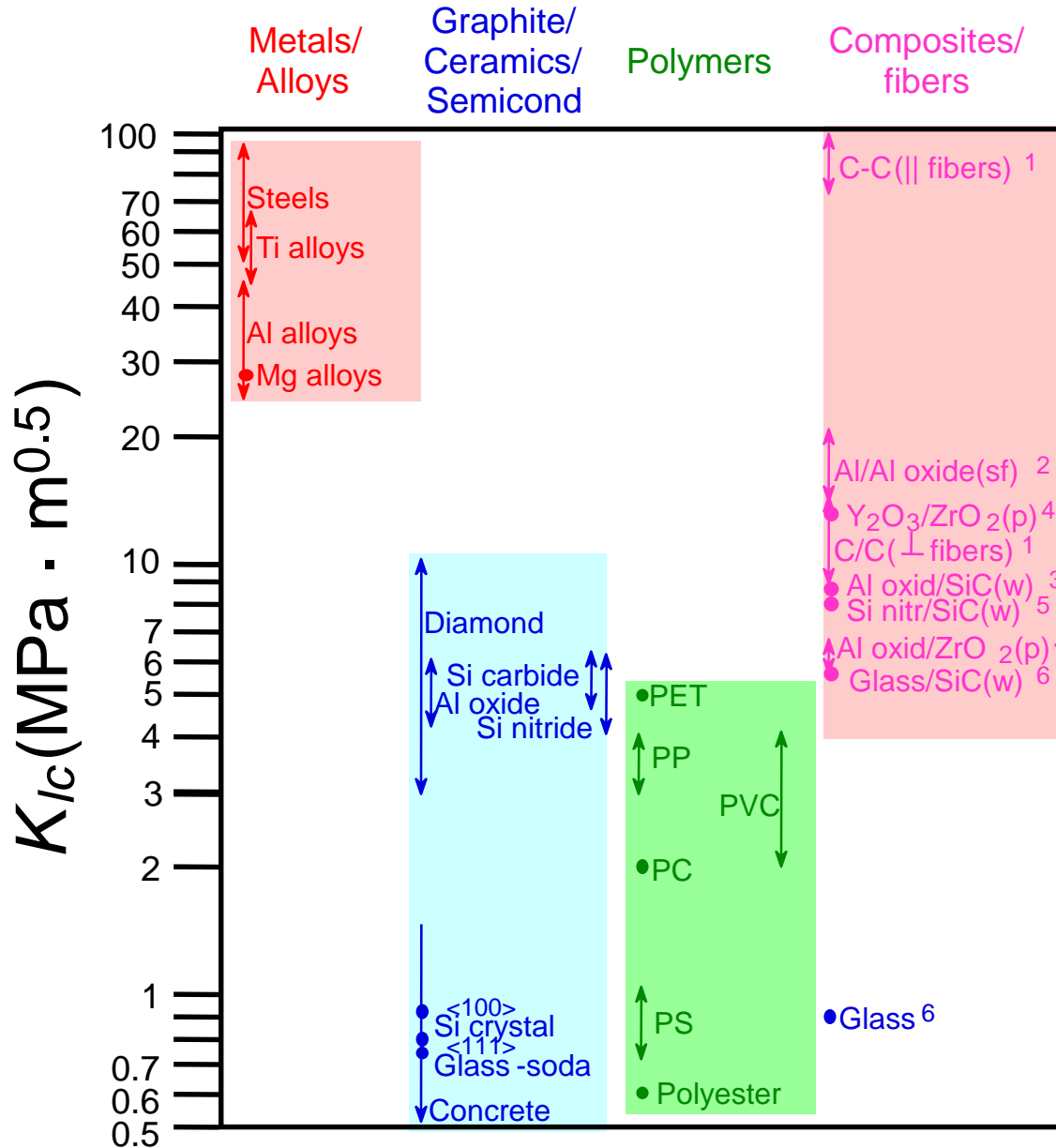
$$K_{Ic} = Y\sigma\sqrt{\pi a}$$



Fracture Toughness

- **Brittle materials do not undergo large plastic deformation, so they possess low K_{IC} than ductile ones.**
- **K_{IC} increases with increase in temp and with reduction in grain size if other elements are held constant**
- **K_{IC} reduces with increase in strain rate**

Fracture Toughness



$$K_{Ic} = Y\sigma\sqrt{\pi a}$$

Design Example: Aircraft Wing

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Design B

- use same material
- largest flaw is 4 mm
- failure stress = ?

- Use...

$$\sigma_c = \frac{K_c}{Y \sqrt{\pi a}}$$

- Key point: Y and K_c are the same in both designs.

--Result:

$$\left(\overset{112 \text{ MPa}}{\sigma_c} \sqrt{\overset{9 \text{ mm}}{a}} \right)_A = \left(\sigma_c \sqrt{a} \right)_B \overset{4 \text{ mm}}{\leftarrow}$$

Answer: $(\sigma_c)_B = 168 \text{ MPa}$

- Reducing flaw size pays off!