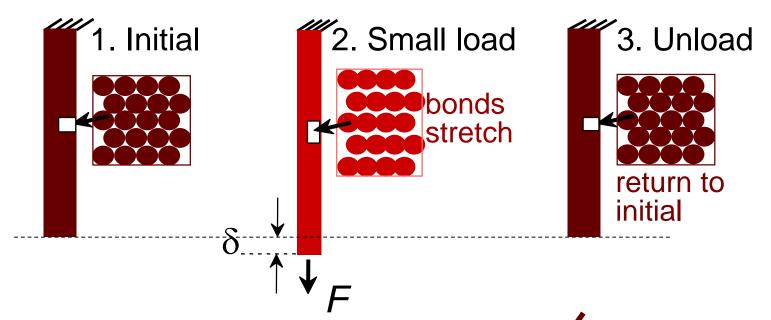
## Mechanical Properties

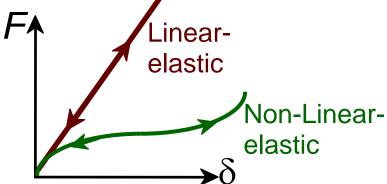
#### ISSUES TO COVERED

- Stress and strain: What are they and why are they used instead of load and deformation?
- Elastic behavior: When loads are small, how much deformation occurs? What materials deform least?
- Plastic behavior: At what point does permanent deformation occur? What materials are most resistant to permanent deformation?
- Toughness and ductility: What are they and how do we measure them?

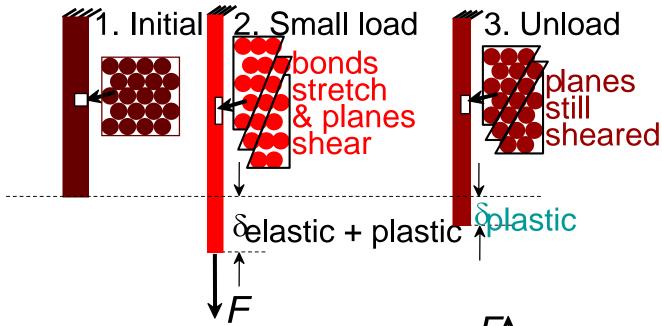
### Elastic Deformation



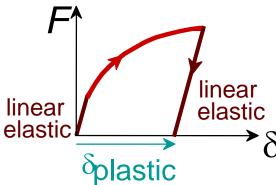
Elastic means reversible!



## Plastic Deformation (Metals)

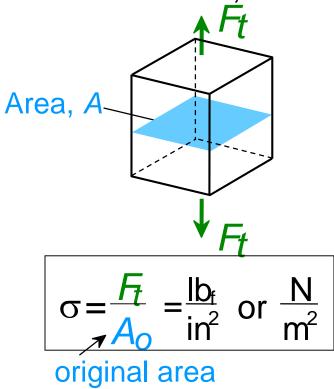


Plastic means permanent!

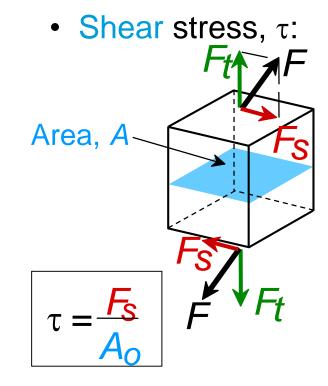


## **Engineering Stress**

• Tensile stress, σ:



before loading



.. Stress has units: N/m<sup>2</sup> or lb<sub>f</sub>/in<sup>2</sup>

#### Common States of Stress

Simple tension: cable -



 $A_0$  = cross sectional area (when unloaded)

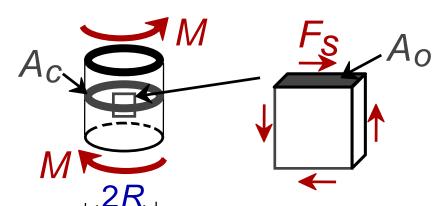
$$\sigma = \frac{F}{A_O} \quad \sigma$$



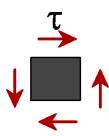


• Torsion (a form of shear): drive shaft

Ski lift (photo courtesy P.M. Anderson)



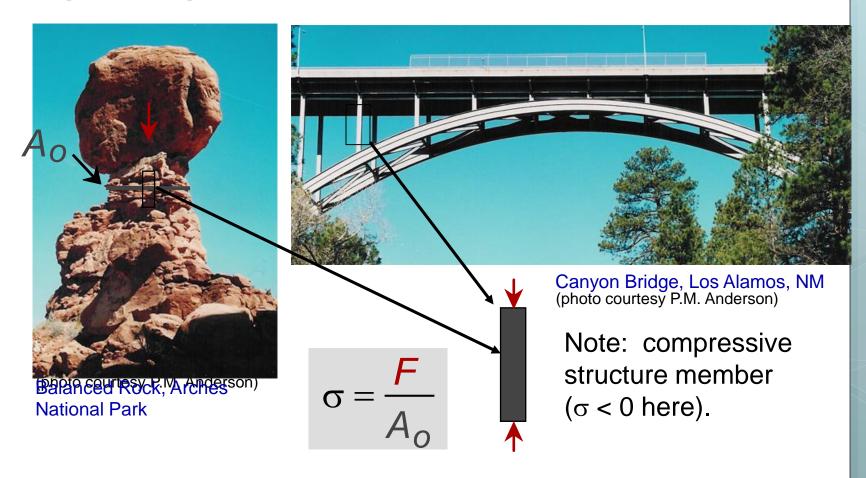
$$\tau = \frac{F_S}{A_O}$$



Note:  $\tau = M/A_cR$  here.

#### OTHER COMMON STRESS STATES (1)

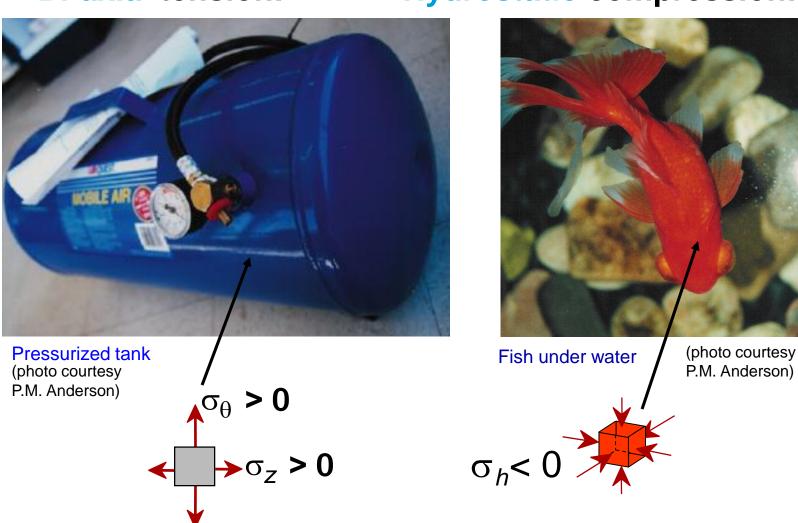
#### **Simple compression:**



#### OTHER COMMON STRESS STATES (2)

• Bi-axial tension:

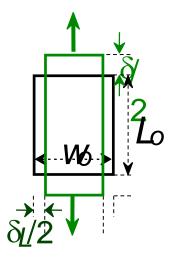
• Hydrostatic compression:



## **Engineering Strain**

• Tensile strain:

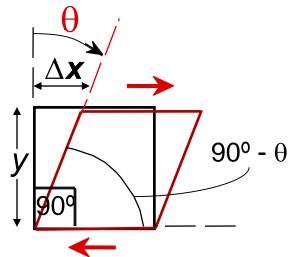
$$\varepsilon = \frac{\delta}{L_o}$$



Lateral strain:

$$\varepsilon_L = -\frac{\delta L}{W_o}$$

• Shear strain:

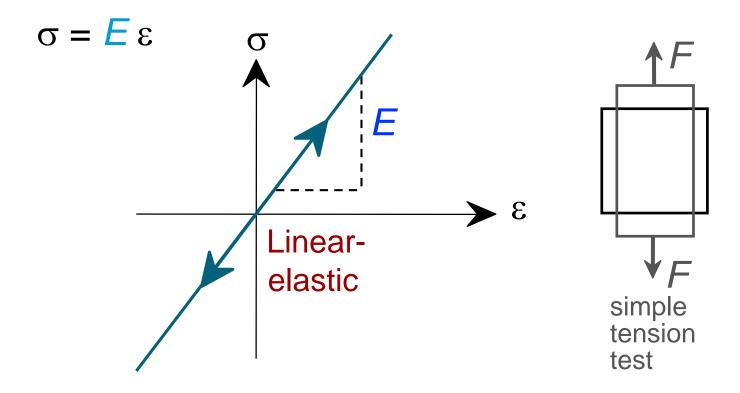


$$\gamma = \Delta x/y = \tan \theta$$

Strain is always dimensionless.

#### Linear Elastic Properties

- Modulus of Elasticity, E: (also known as Young's modulus)
- Hooke's Law:



• A piece of copper originally **305mm** (12 in.) long is pulled in tension with a stress of **276MPa** (40,000psi). If the deformation is entirely elastic, what will be the resultant elongation?

$$\sigma = \epsilon E = \left(\frac{\Delta l}{l_0}\right) E$$

$$\Delta l = \frac{\sigma l_0}{E}$$

• Magnitude of E for copper from Table 6.1 is 110 GPa

$$\Delta l = \frac{(276 \text{ MPa})(305 \text{ mm})}{110 \times 10^3 \text{ MPa}} = 0.77 \text{ mm} (0.03 \text{ in.})$$

A tensile stress is to be applied along the long axis of a cylindrical brass rod that has a diameter of 10mm. Determine the magnitude of the load required to produce a 0.0025mm change in

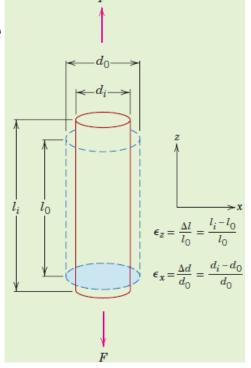
diameter if the deformation is entire

For the strain in the x direction:

$$\epsilon_x = \frac{\Delta d}{d_0} = \frac{-2.5 \times 10^{-3} \text{ mm}}{10 \text{ mm}} = -2.5 \times 10^{-4}$$

$$\epsilon_z = -\frac{\epsilon_x}{\nu} = -\frac{(-2.5 \times 10^{-4})}{0.34} = 7.35 \times 10^{-4}$$

$$\sigma = \epsilon_z E = (7.35 \times 10^{-4})(97 \times 10^3 \text{ MPa}) = 71.3 \text{ MPa}$$



$$F = \sigma A_0 = \sigma \left(\frac{d_0}{2}\right)^2 \pi$$

= 
$$(71.3 \times 10^6 \text{ N/m}^2) \left(\frac{10 \times 10^{-3} \text{ m}}{2}\right)^2 \pi = 5600 \text{ N}$$

#### Poisson's ratio, v

 Poisson's ratio, v:is defined as the ratio of the lateral and axial strains

$$\nu = -\frac{\epsilon_x}{\epsilon_z} = -\frac{\epsilon_y}{\epsilon_z}$$

metals:  $v \sim 0.33$ 

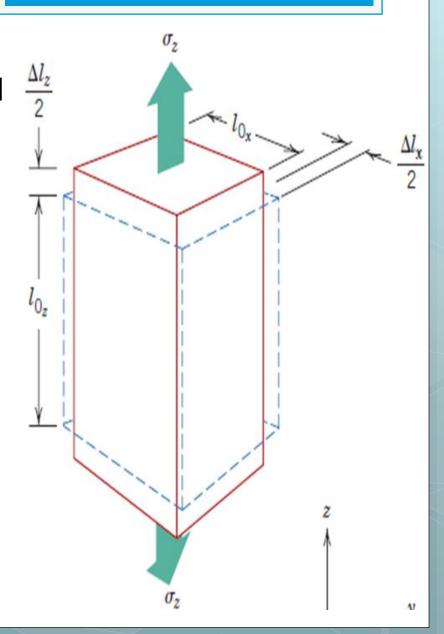
ceramics:  $v \sim 0.25$ 

polymers:  $v \sim 0.40$ 

Units:

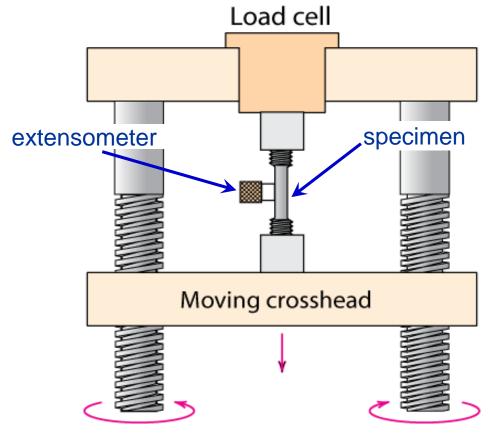
*E*: [GPa] or [psi]

v: dimensionless



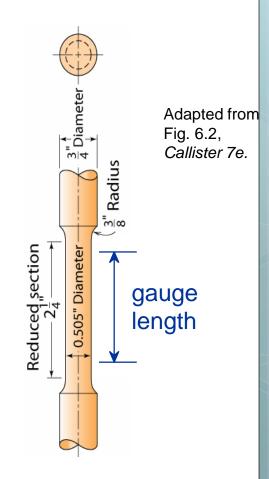
#### Stress-Strain Testing

 Typical tensile test machine



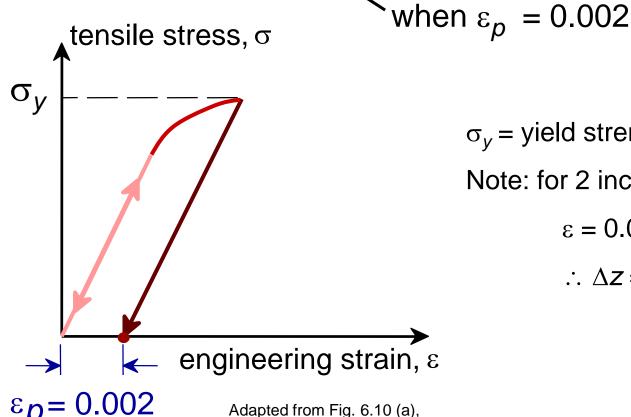
Adapted from Fig. 6.3, *Callister 7e.* (Fig. 6.3 is taken from H.W. Hayden, W.G. Moffatt, and J. Wulff, *The Structure and Properties of Materials*, Vol. III, *Mechanical Behavior*, p. 2, John Wiley and Sons, New York, 1965.)

 Typical tensile specimen



## Yield Strength, $\sigma_{V}$

 Stress at which noticeable plastic deformation has occurred.



Callister 7e.

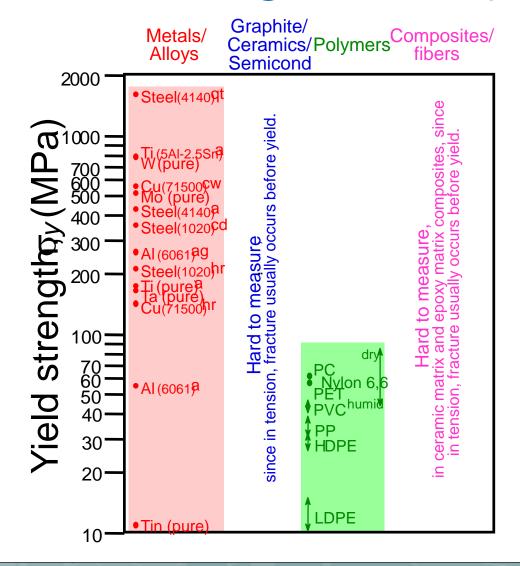
 $\sigma_v$  = yield strength

Note: for 2 inch sample

$$\varepsilon = 0.002 = \Delta z/z$$

$$\Delta z = 0.004$$
 in

## Yield Strength: Comparison



#### Room T values

Based on data in Table B4, *Callister 7e*.

a = annealed

hr = hot rolled

ag = aged

cd = cold drawn

cw = cold worked

gt = quenched & tempered

#### Plastic (Permanent) Deformation

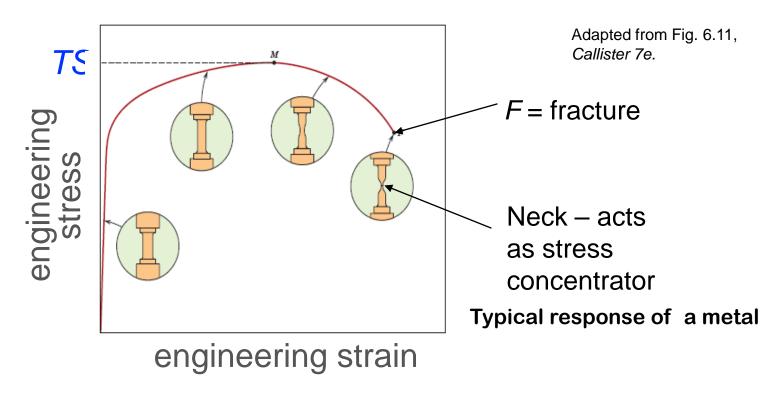
(at lower temperatures, i.e.  $T < T_{melt}/3$ )

• Simple tension test: Elastic+Plastic engineering stress, σ 1 at larger stress **Elastic** initial permanent (plastic) after load is removed engineering strain, ε

Adapted from Fig. 6.10 (a), *Callister 7e.* 

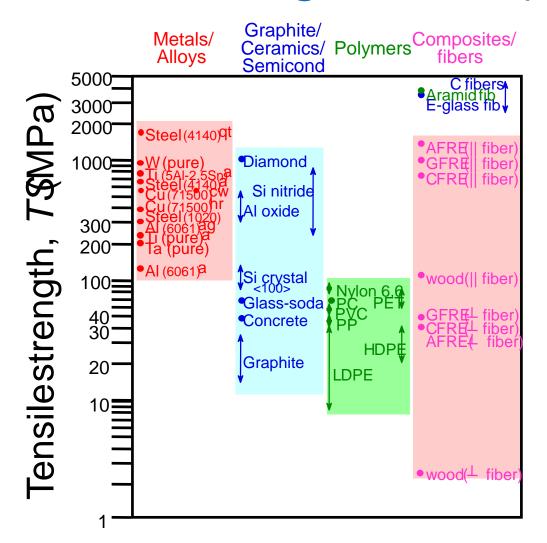
## Tensile Strength, TS

• Maximum stress on engineering stress-strain curve.



- Metals: occurs when noticeable necking starts.
- Polymers: occurs when polymer backbone chains are aligned and about to break.

## Tensile Strength: Comparison



#### Room Temp. values

Based on data in Table B4, Callister 7e.

a = annealed

hr = hot rolled

ag = aged

cd = cold drawn

cw = cold worked

qt = quenched & tempered

AFRE, GFRE, & CFRE = aramid, glass, & carbon fiber-reinforced epoxy composites, with 60 vol% fibers.

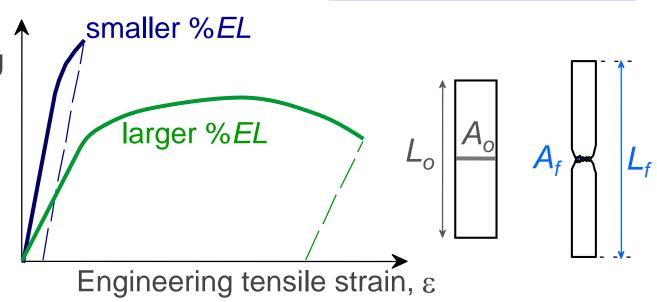
## Ductility

Plastic tensile strain at failure:

$$\%EL = \frac{L_f - L_o}{L_o} \times 100$$

Engineering tensile stress,  $\sigma$ 

Adapted from Fig. 6.13, *Callister 7e.* 



• Another ductility measure:

$$%RA = \frac{A_o - A_f}{A_o} \times 100$$

- A cylindrical specimen of steel having an original diameter of 12.8mm is tensile tested to fracture and found to have an engineering fracture strength  $\sigma_{\rm f}$  of 460MPa. If its cross-sectional diameter at fracture is 10.7mm, determine:
- (a) The ductility in terms of percent reduction in area
- (b) The true stress at fracture

Ductility is computed as

$$\% RA = \frac{\left(\frac{12.8 \text{ mm}}{2}\right)^2 \pi - \left(\frac{10.7 \text{ mm}}{2}\right)^2 \pi}{\left(\frac{12.8 \text{ mm}}{2}\right)^2 \pi} \times 100$$

$$= \frac{128.7 \text{ mm}^2 - 89.9 \text{ mm}^2}{128.7 \text{ mm}^2} \times 100 = 30\%$$

True stress is defined by Equation  $\sigma_T = \frac{r}{A_i}$  where the area is taken as the fracture area  $A_f$  However, the load at fracture must first be

computed from the fracture strength as

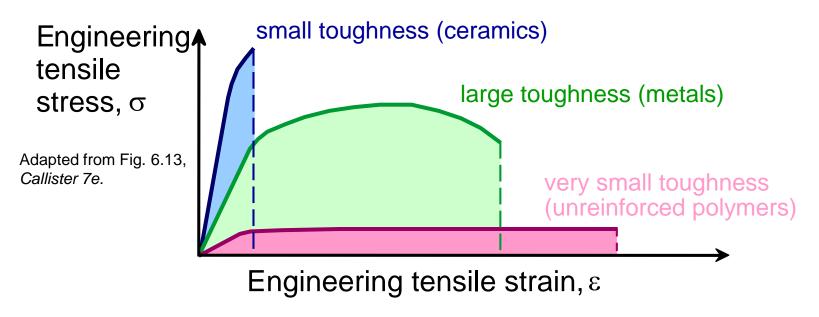
$$F = \sigma_f A_0 = (460 \times 10^6 \text{ N/m}^2)(128.7 \text{ mm}^2) \left(\frac{1 \text{ m}^2}{10^6 \text{ mm}^2}\right) = 59,200 \text{ N}$$

And the true stress is calculated as

$$\sigma_T = \frac{F}{A_f} = \frac{59,200 \text{ N}}{(89.9 \text{ mm}^2) \left(\frac{1 \text{ m}^2}{10^6 \text{ mm}^2}\right)} = 6.6 \times 10^8 \text{ N/m}^2 = 660 \text{ MPa}$$

## Toughness

- Energy to break a unit volume of material
- Approximate by the area under the stress-strain curve.



Brittle fracture: elastic energy

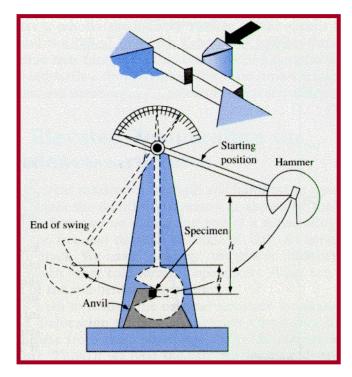
Ductile fracture: elastic + plastic energy

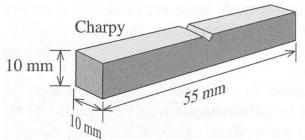
## **Impact Fracture Testing**

In an impact test, a notched specimen is fractured by an impact blow, and the energy absorbed during the fracture is measured.

There are two types of tests – Charpy impact test and Izod impact test.

## **Impact Test: The Charpy Test**

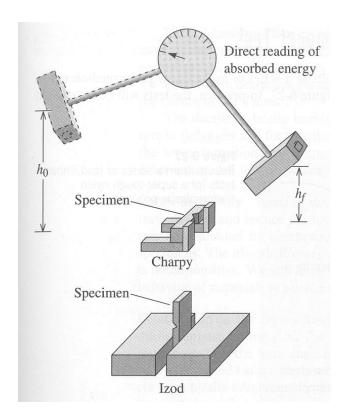


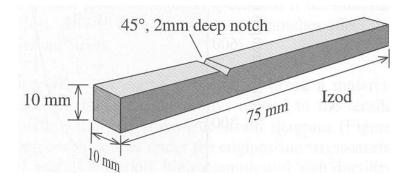


The ability of a material to withstand an impact blow is referred to as notch toughness.

The energy absorbed is the difference in height between initial and final position of the hammer. The material fractures at the notch and the structure of the cracked surface will help indicate whether it was a brittle or ductile fracture.

### **Impact Test: The Izod Test**





Generally used for polymers. Izod test is different from the Charpy test in terms of the configuration of the notched test specimen

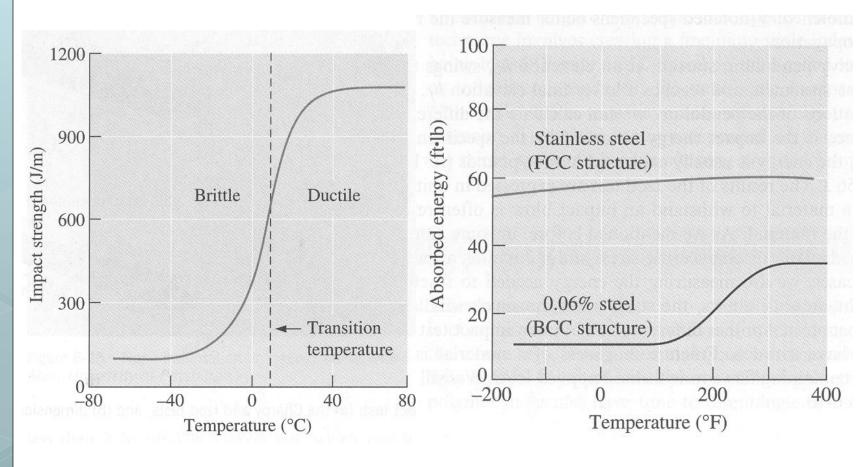
### **Impact Tests: Test conditions**

- The FCC alloys→ generally ductile fracture mode
- The HCP alloys→ generally brittle fracture mode
- Temperature is important
- The BCC alloys→ brittle modes at relatively low temperatures and ductile mode at relatively high temperature

## **Transition Temperatures**

- As temperature decreases a ductile material can become brittle - ductile-to-brittle transition
  - The transition temperature is the temp at which a material changes from ductile-to-brittle behavior

#### **Ductile to Brittle Transition**



#### True Stress & Strain

Note: S.A. changes when sample stretched

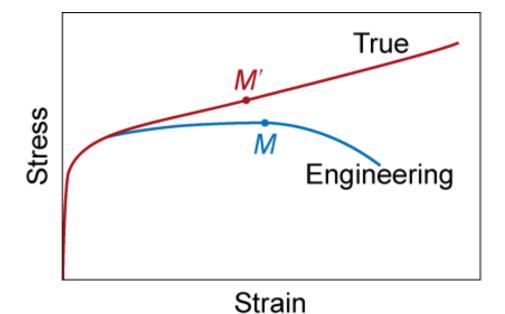
$$\sigma_T = F/A_i$$

$$\varepsilon_T = \ln(\ell_i/\ell_o)$$

$$\sigma_{T} = \sigma(1+\varepsilon)$$

$$\varepsilon_{T} = \ln(1+\varepsilon)$$

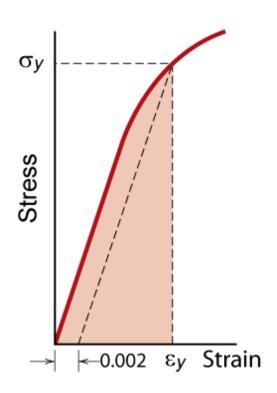
$$\varepsilon_{\tau} = \ln(1+\varepsilon)$$



Adapted from Fig. 6.16, Callister 7e.

## Modulus of Resilience, $U_R$

- Ability of a material to store energy
- Energy stored best in elastic region



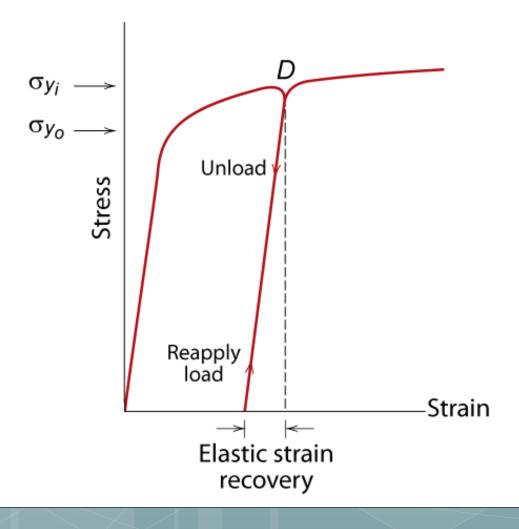
$$U_R = \int_0^{\varepsilon_y} \sigma d\varepsilon$$

If we assume a linear stress-strain curve this simplifies to

$$U_R \cong \frac{1}{2} \sigma_y \varepsilon_y$$

Adapted from Fig. 6.15, *Callister 7e.* 

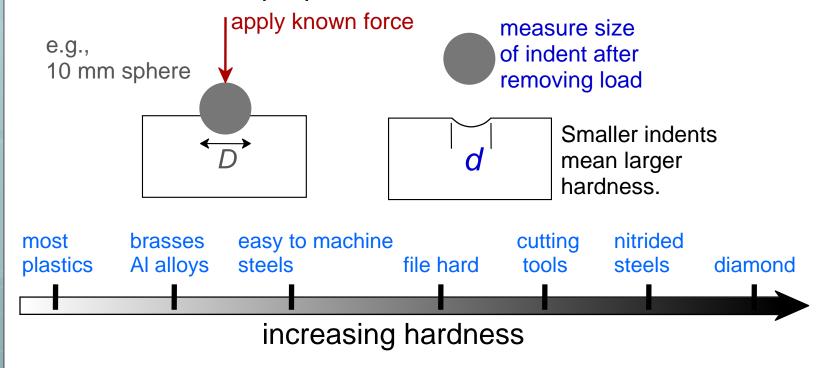
## Elastic Strain Recovery



Adapted from Fig. 6.17, *Callister 7e.* 

#### Hardness

- Resistance to permanently indenting the surface.
- Large hardness means:
  - --resistance to plastic deformation or cracking in compression.
  - --better wear properties.



## Hardness: Measurement

- Rockwell
  - No major sample damage
  - Each scale runs to 130 but only useful in range 20-100.
  - Minor load 10 kg
  - Major load
     60 (A), 100 (B) & 150 (C) kg
    - A = diamond, B = 1/16 in. ball, C = diamond
- HB = Brinell Hardness
  - TS (psia) =  $500 \times HB$
  - $TS (MPa) = 3.45 \times HB$

Table 6.5 Hardness Testing Techniques

		Shape of Indentation			Formula for
Test	Indenter	Side View	Top View	Load	Hardness Numbera
Brinell	10-mm sphere of steel or tungsten carbide	→ D ← d ←	<u>⇒</u> d =	P	$HB = \frac{2P}{\pi D[D - \sqrt{D^2 - d^2}]}$
Vickers microhardness	Diamond pyramid	136°	$d_1$ $d_1$	P	$HV = 1.854P/d_1^2$
Knoop microhardness	Diamond pyramid	## ## ## ## ## ## ## ## ## ## ## ## ##	b	P	$HK = 14.2P/l^2$
Rockwell and Superficial Rockwell	$\begin{cases} \text{Diamond} \\ \text{cone} \\ \frac{1}{18}, \frac{1}{8}, \frac{1}{4}, \frac{1}{2} \text{ in.} \\ \text{diameter} \\ \text{steel spheres} \end{cases}$	120°		100 150 15 30	kg kg Rockwell kg kg Superficial Rockwell kg

<sup>&</sup>lt;sup>a</sup> For the hardness formulas given, P (the applied load) is in kg, while D, d, d, and l are all in mm. **Source:** Adapted from H. W. Hayden, W. G. Moffatt, and J. Wulff, *The Structure and Properties of Materials*, Vol. III, *Mechanical Behavior*. Copyright © 1965 by John Wiley & Sons, New York. Reprinted by permission of John Wiley & Sons, Inc.

#### Hardness of Metals and Ceramics

Material	Vickers Hardness, HV	Knoop Hardness, HK
Hardened tool steel <sup>a</sup>	800	850
Cemented carbide (WC - Co)2	2000	1400
Alumina, Al <sub>2</sub> O <sub>3</sub>	2200	1500
Tungsten carbide, WC	2600	1900
Silicon carbide, SiC	2600	1900

Material	Vickers Hardness, HV	Knoop Hardness, HK
Titanium nitride, TiN	3000	2300
Titanium carbide, TiC	3200	2500
Cubic boron nitride, BN	6000	4000
Diamond, sintered polycrystal	7000	5000
Diamond, natural	10,000	8000

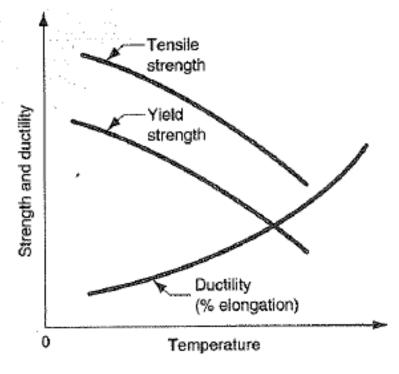
# **Hardness of Polymers**

Polymer	Brinell Hardness, HB		
Nylon	12		
Phenol formaldehyde	50		
Polyethylene, low density	2		
Polyethylene, high density	4		
Polymer	Brinell Hardness, HB		
Polymer Polypropylene	2000		
	2000		

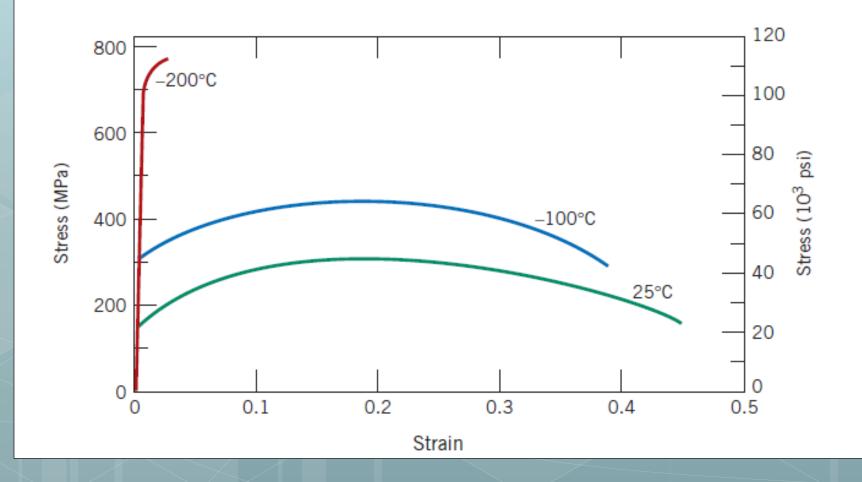
# Effect of Temperature on Mechanical Properties

 Generally speaking, materials are lower in strength and higher in ductility, at elevated

temperatures

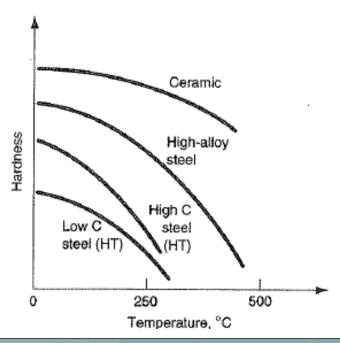


# Engineering stress-strain behavior for Iron at three temperatures



#### **Hot Hardness**

- A property used to characterize strength and hardness at elevated temperatures is Hot Hardness
- It is the ability of a material to retain its hardness at elevated temperatures



## Summary

- Stress and strain: These are size-independent measures of load and displacement, respectively.
- Elastic behavior: This reversible behavior often shows a linear relation between stress and strain.
   To minimize deformation, select a material with a large elastic modulus (E or G).
- Plastic behavior: This permanent deformation behavior occurs when the tensile (or compressive) uniaxial stress reaches  $\sigma_v$ .
- Toughness: The energy needed to break a unit volume of material.
- Ductility: The plastic strain at failure.