

**Phase Diagrams**  
**Binary Eutectoid Systems**  
**and**  
**Fe-C phase Diagram**

# What is Phase?

- The term 'phase' refers to a separate and identifiable state of matter in which a given substance may exist.
- Applicable to both crystalline and non-crystalline materials
- An important refractory oxide **silica** is able to exist as three crystalline phases, **quartz**, **tridymite** and **crystalobalite**, as well as a non-crystalline phase, **silica glass**, and as **molten silica**
- Every pure material is considered to be a phase, so also is every solid, liquid, and gaseous solution
- For example, the **sugar–water** syrup solution is one phase, and solid sugar is another

# Introduction to Phase Diagram

- There is a strong correlation between **microstructure** and **mechanical properties**, and the development of microstructure of an alloy is related to the characteristics of its [phase diagram](#)
- It is a type of chart used to show conditions at which thermodynamically distinct phases can occur at equilibrium
- Provides valuable information about melting, casting, crystallization, and other phenomena

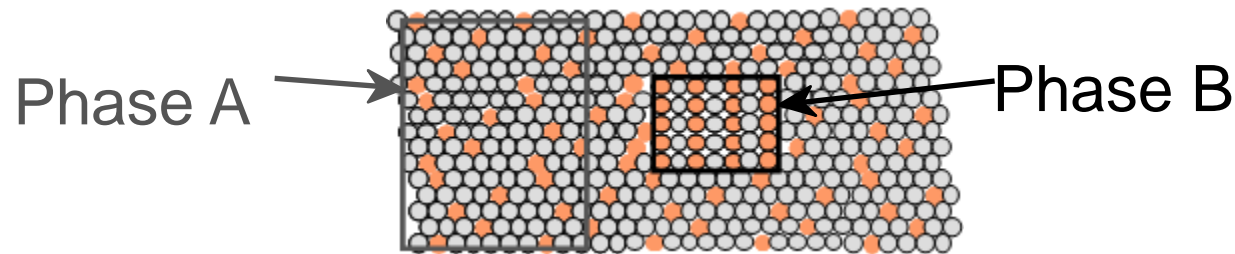
# ISSUES TO ADDRESS...

- When we combine two elements...  
what equilibrium state do we get?
- In particular, if we specify...  
--a composition (e.g., wt% Cu - wt% Ni), and  
--a temperature ( $T$ )

then...

How many phases do we get?

What is the composition of each phase? How much of each phase do we get?

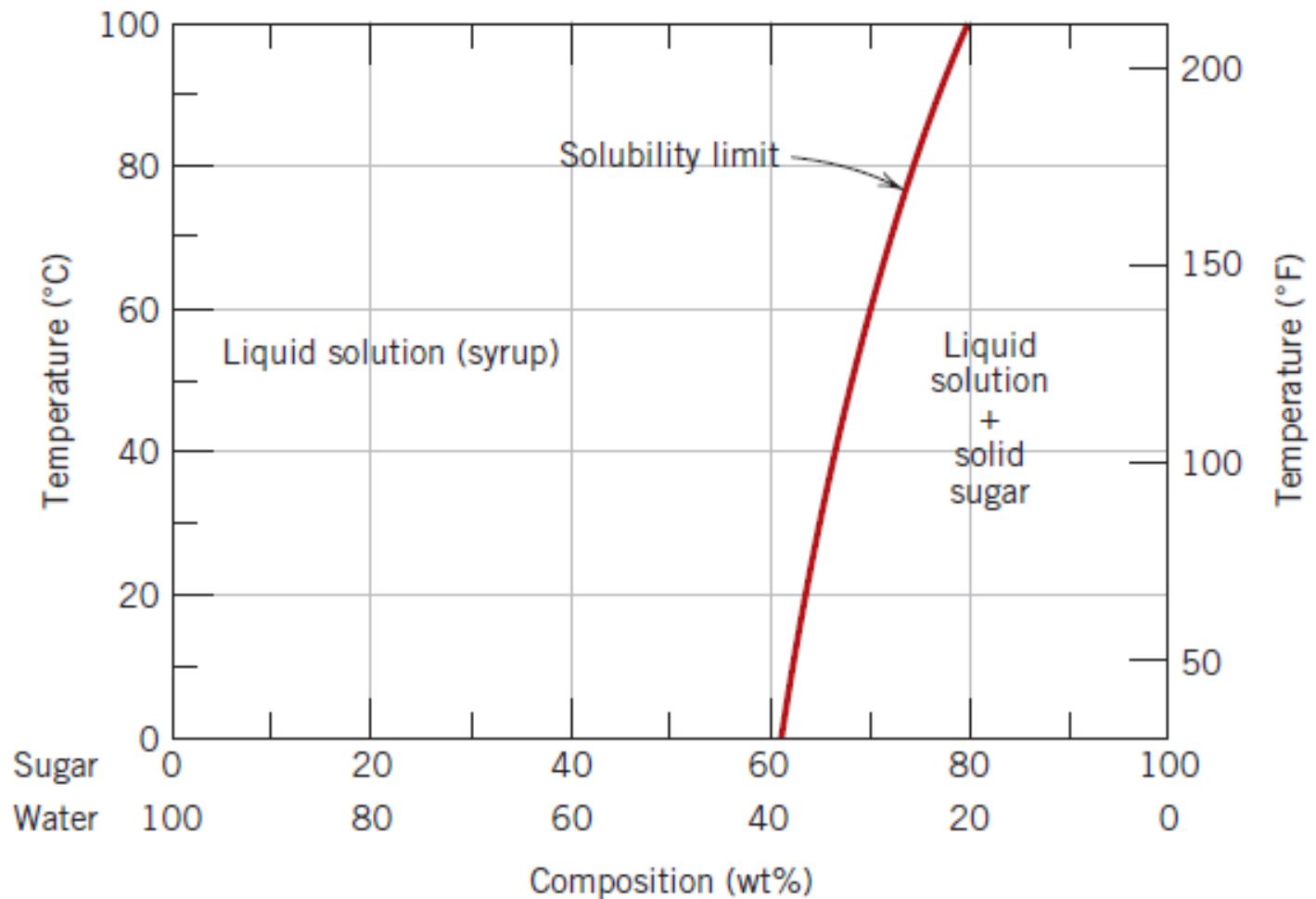


- Nickel atom
- Copper atom

# Solubility Limit

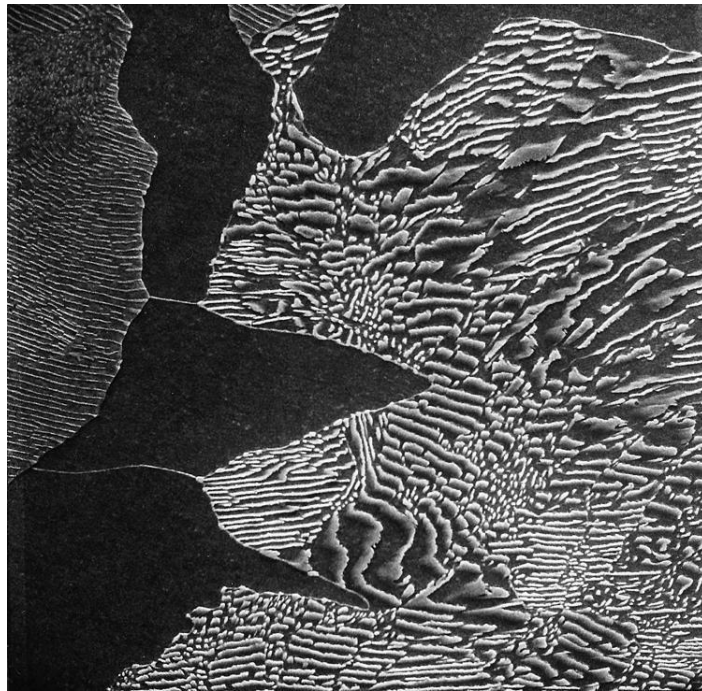
- At some specific temperature, there is a maximum concentration of **solute** atoms that may dissolve in the **solvent** to form a solid solution, which is called as Solubility Limit
- The addition of solute in excess of this solubility limit results in the formation of another compound that has a distinctly different composition
- This solubility limit depends on the temperature

# Solubility Limit Sugar-Water



# Microstructure

- the structure of a prepared surface of material as revealed by a microscope above **25×** magnification
- The microstructure of a material can strongly influence properties such as strength, toughness, ductility, hardness, corrosion resistance, high/low temperature behavior, wear resistance, etc



# Components and Phases

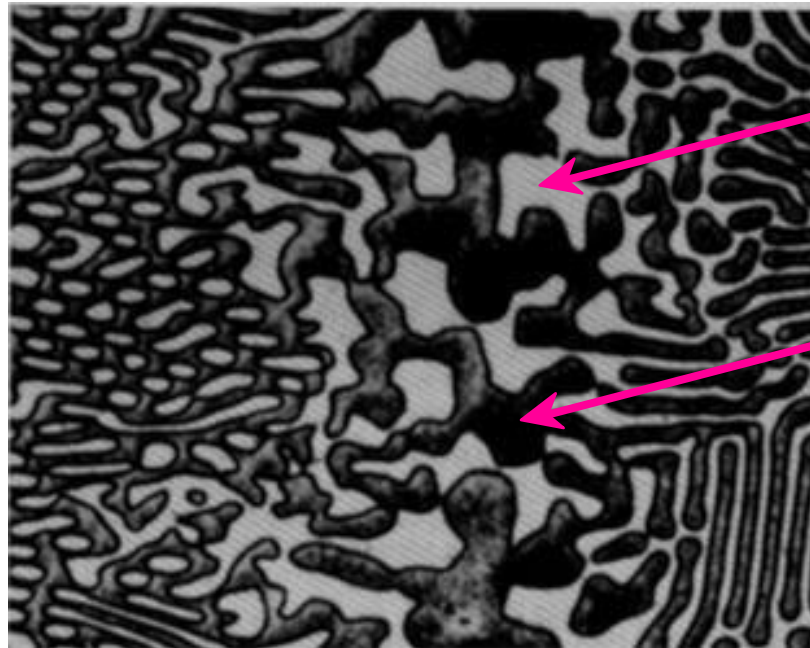
- **Components:**

The elements or compounds which are present in the mixture (e.g., Al and Cu)

- **Phases:**

The physically and chemically distinct material regions that result (e.g.,  $\alpha$  and  $\beta$ ).

Aluminum-  
Copper  
Alloy



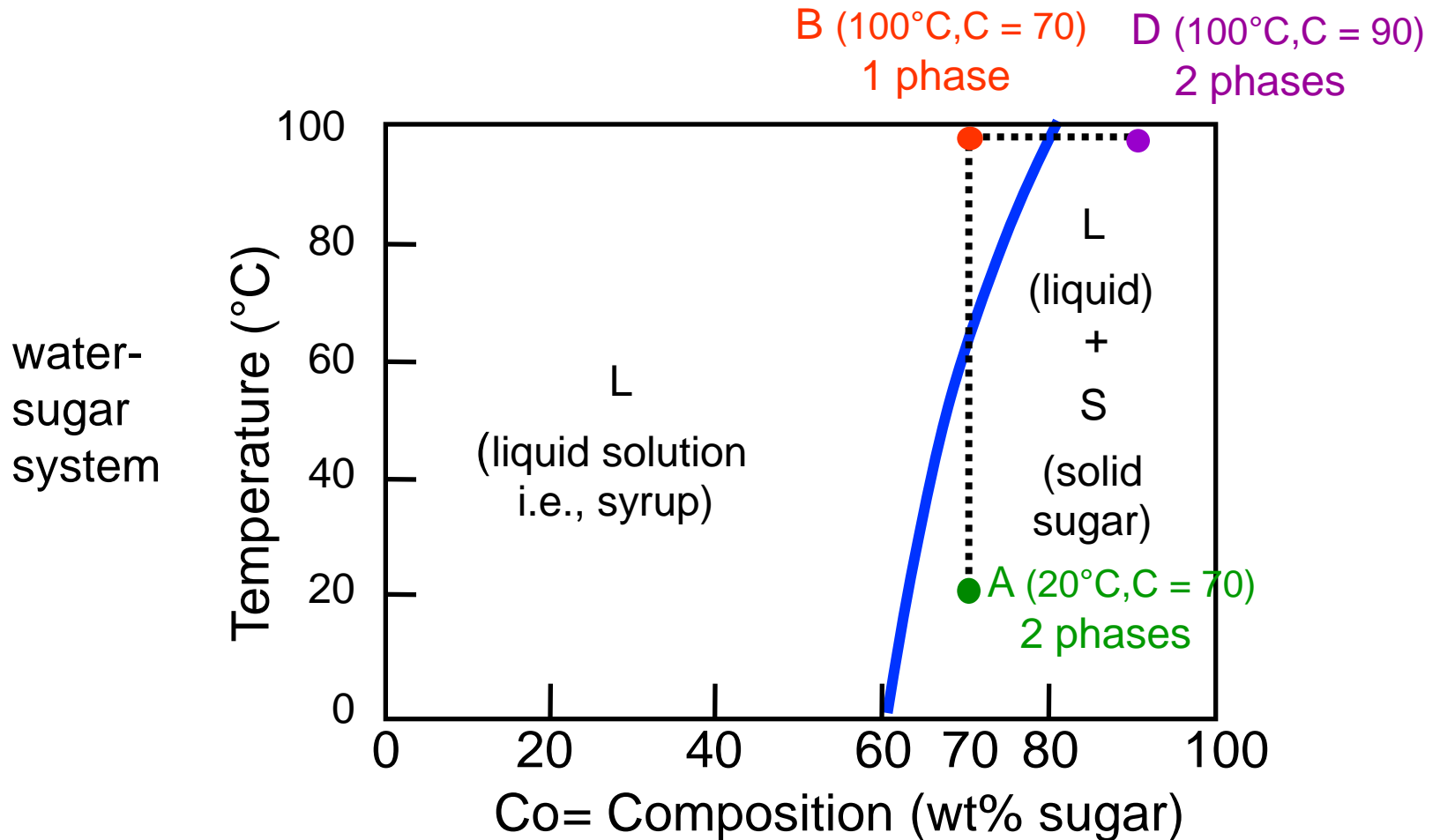
$\beta$  (lighter  
phase)

$\alpha$   
(darker  
phase)



# Effect of Temperature T & Composition Co

- Altering T can change # of phases: path A to B.
- Altering C can change # of phases: path B to D.



# Binary Phase Diagrams

- A phase diagram in which **temperature** and **composition** are variable parameters, and **pressure** is held constant—normally **1 atm**
- **Binary phase diagrams** are maps that represent the relationships between **temperature** and the **compositions** and quantities of phases at equilibrium, which influence the microstructure of an alloy.
- Many **microstructures** develop from phase transformations, the changes that occur when the **temperature** is altered

# Phase Equilibria

Simple solution system (e.g., Ni-Cu solution)

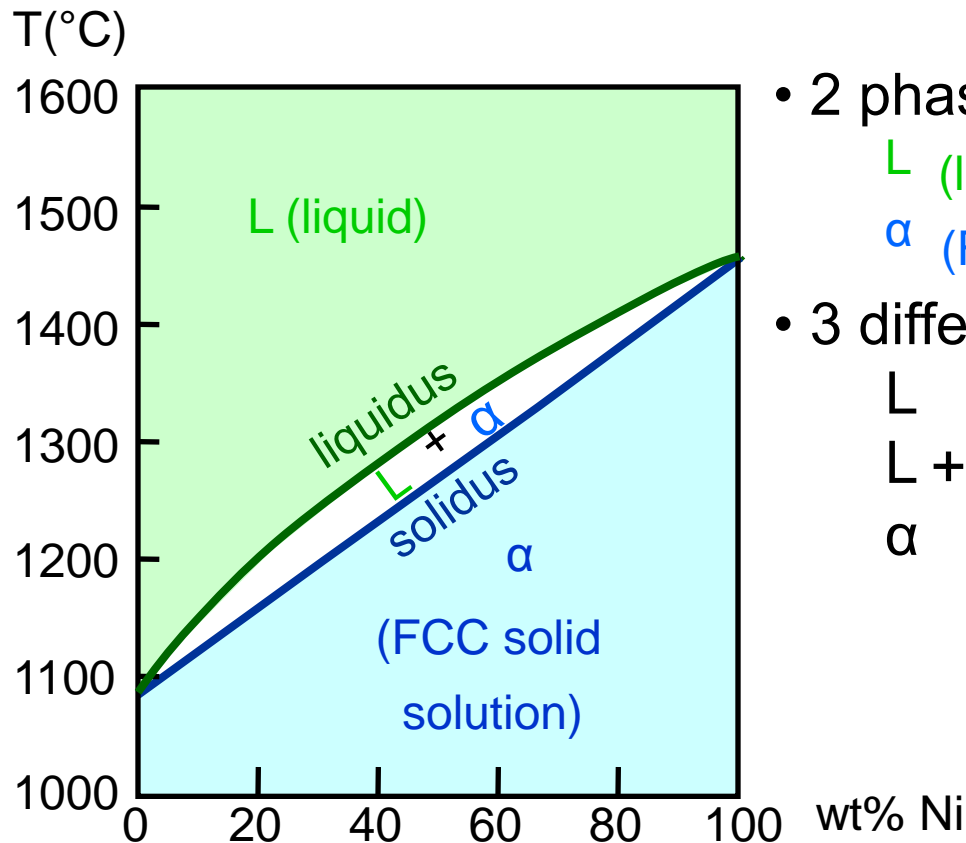
|    | Crystal Structure | electroneg | $r$ (nm) |
|----|-------------------|------------|----------|
| Ni | FCC               | 1.9        | 0.1246   |
| Cu | FCC               | 1.8        | 0.1278   |

- Both have the same crystal structure (FCC) and have similar electronegativities and atomic radii ([W. Hume – Rothery rules](#)) suggesting high mutual solubility.
- Ni and Cu are totally miscible in all proportions.

# Phase Diagrams

- Indicate phases as a function of T, C, and P.
- For this course:
  - binary systems: just 2 components.
  - independent variables: T and C (P = 1 atm is almost always used).

Phase Diagram for Cu-Ni system



- 2 phases:
  - L (liquid)
  - α (FCC solid solution)
- 3 different phase fields:
  - L
  - L + α
  - α

# Phase Diagrams:

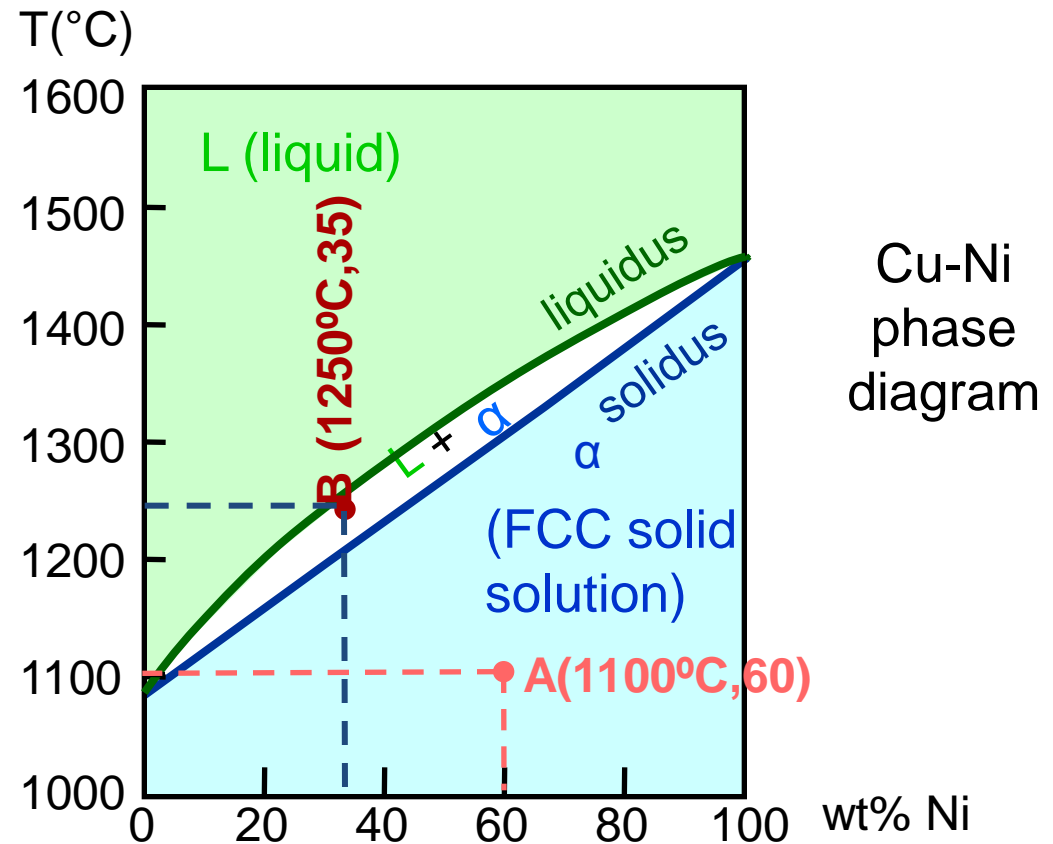
## Determination of phase(s) present

- Rule 1: If we know  $T$  and  $C_0$ , then we know:
  - which phase(s) is (are) present.

- Examples:

A(1100°C, 60 wt% Ni):  
1 phase:  $\alpha$

B(1250°C, 35 wt% Ni):  
2 phases: L +  $\alpha$



# Phase Diagrams:

## Determination of phase compositions

- Rule 2: If we know  $T$  and  $C_0$ , then we can determine:
  - the composition of each phase.

- Examples:

Consider  $C_0 = 35 \text{ wt\% Ni}$

At  $T_A = 1320^\circ\text{C}$ :

Only Liquid (L) present

$C_L = C_0$  (= 35 wt% Ni)

At  $T_D = 1190^\circ\text{C}$ :

Only Solid ( $\alpha$ ) present

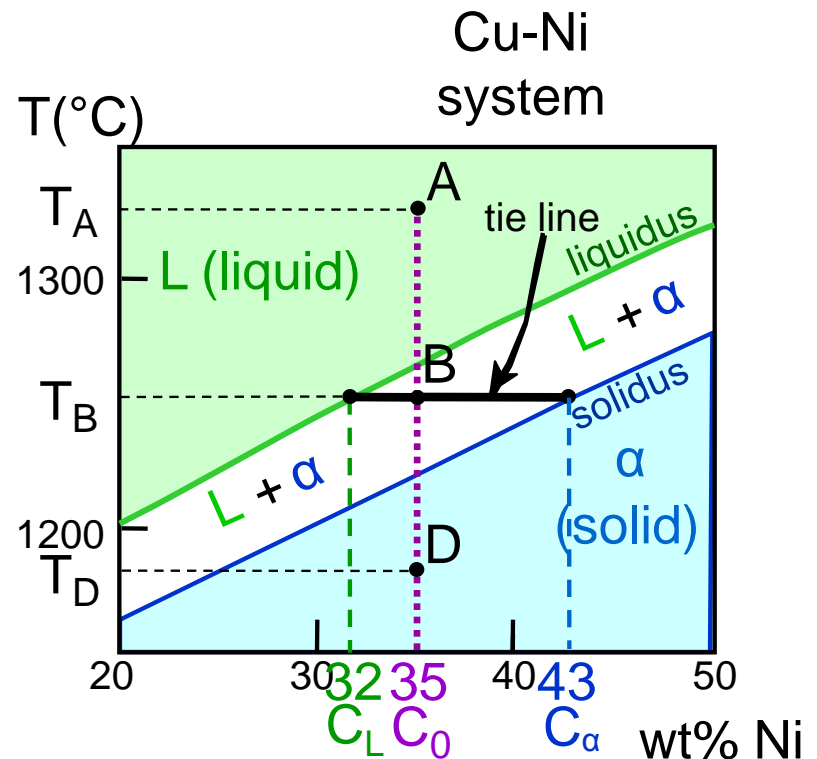
$C_\alpha = C_0$  (= 35 wt% Ni)

At  $T_B = 1250^\circ\text{C}$ :

Both  $\alpha$  and L present

$C_L = C_{\text{liquidus}}$  (= 32 wt% Ni)

$C_\alpha = C_{\text{solidus}}$  (= 43 wt% Ni)



# Phase Diagrams:

## Determination of phase weight fractions

- Rule 3: If we know  $T$  and  $C_0$ , then can determine:
  - the weight fraction of each phase.
- Examples:

Consider  $C_0 = 35 \text{ wt\% Ni}$

At  $T_A$  : Only Liquid (L) present

$$W_L = 1.00, W_\alpha = 0$$

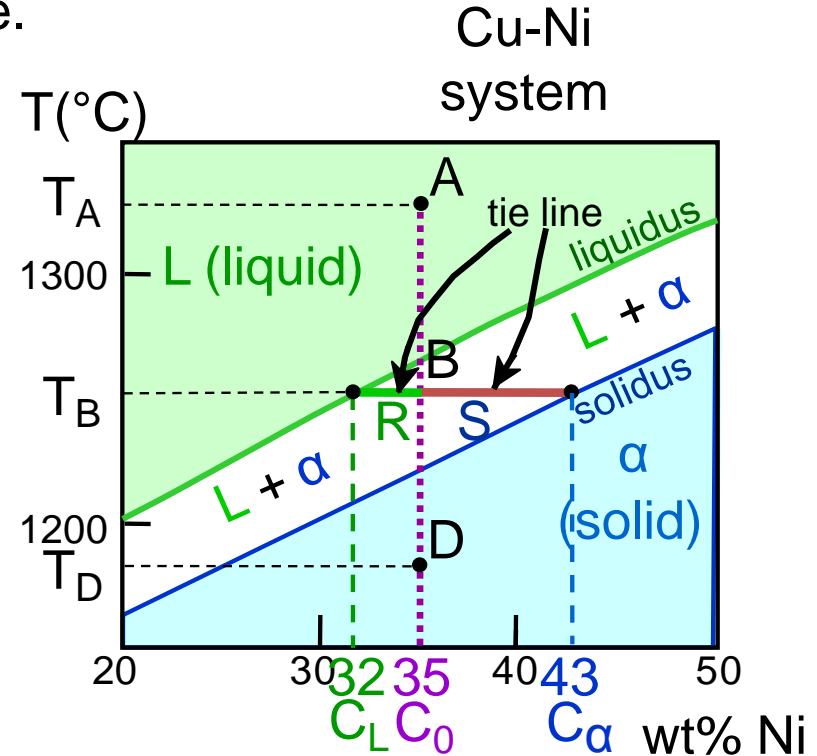
At  $T_D$  : Only Solid ( $\alpha$ ) present

$$W_L = 0, W_\alpha = 1.00$$

At  $T_B$  : Both  $\alpha$  and L present

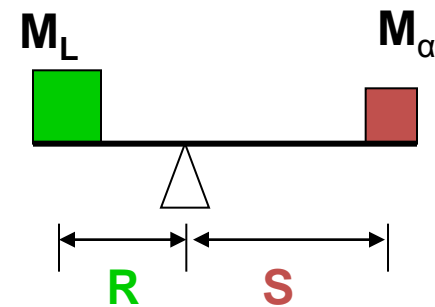
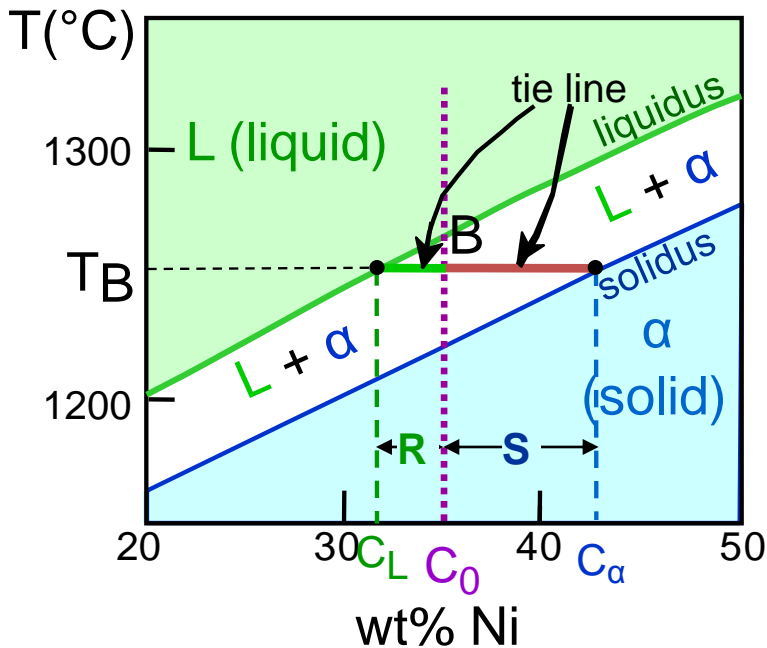
$$W_L = \frac{S}{R + S} = \frac{43 - 35}{43 - 32} = 0.73$$

$$W_\alpha = \frac{R}{R + S} = 0.27$$



# The Lever Rule

Tie line – connects the phases in equilibrium with each other – also sometimes called an isotherm



$$M_\alpha \times S = M_L \times R$$

$$W_L = \frac{M_L}{M_L + M_\alpha} = \frac{S}{R + S} = \frac{C_\alpha - C_0}{C_\alpha - C_L}$$

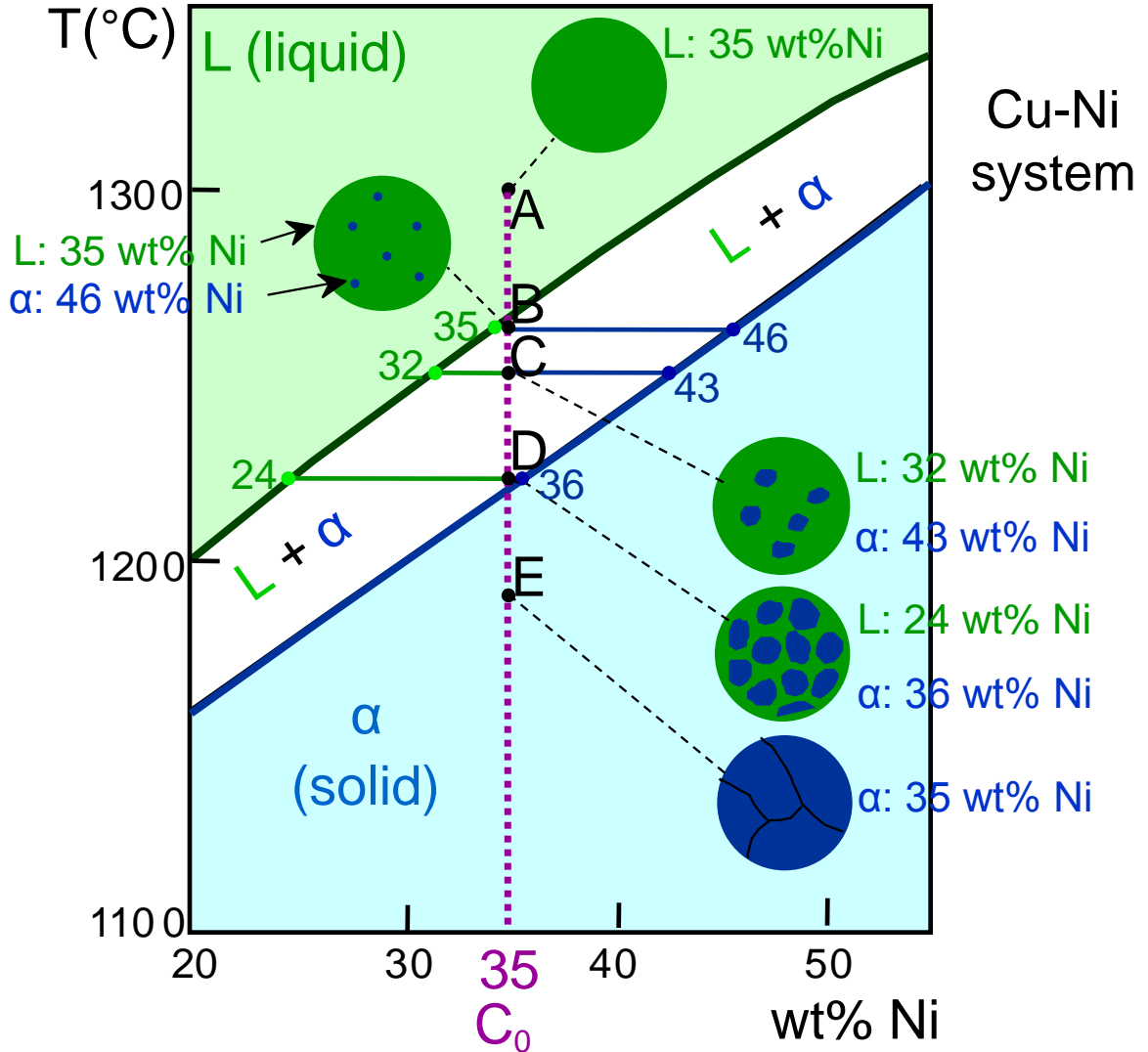
$$W_\alpha = \frac{R}{R + S} = \frac{C_0 - C_L}{C_\alpha - C_L}$$



# Ex: Cooling of a Cu-Ni Alloy

- Phase diagram:  
Cu-Ni system.
- System is:  
--binary  
i.e., 2 components:  
**Cu** and **Ni**.
- isomorphous  
i.e., complete  
solubility of one  
component in  
another; a phase  
field extends from  
0 to 100 wt% Ni.
- Consider  
microstructural  
changes that  
accompany the  
cooling of a

$C_0 = 35 \text{ wt\% Ni}$  alloy



# Equilibrium Cooling

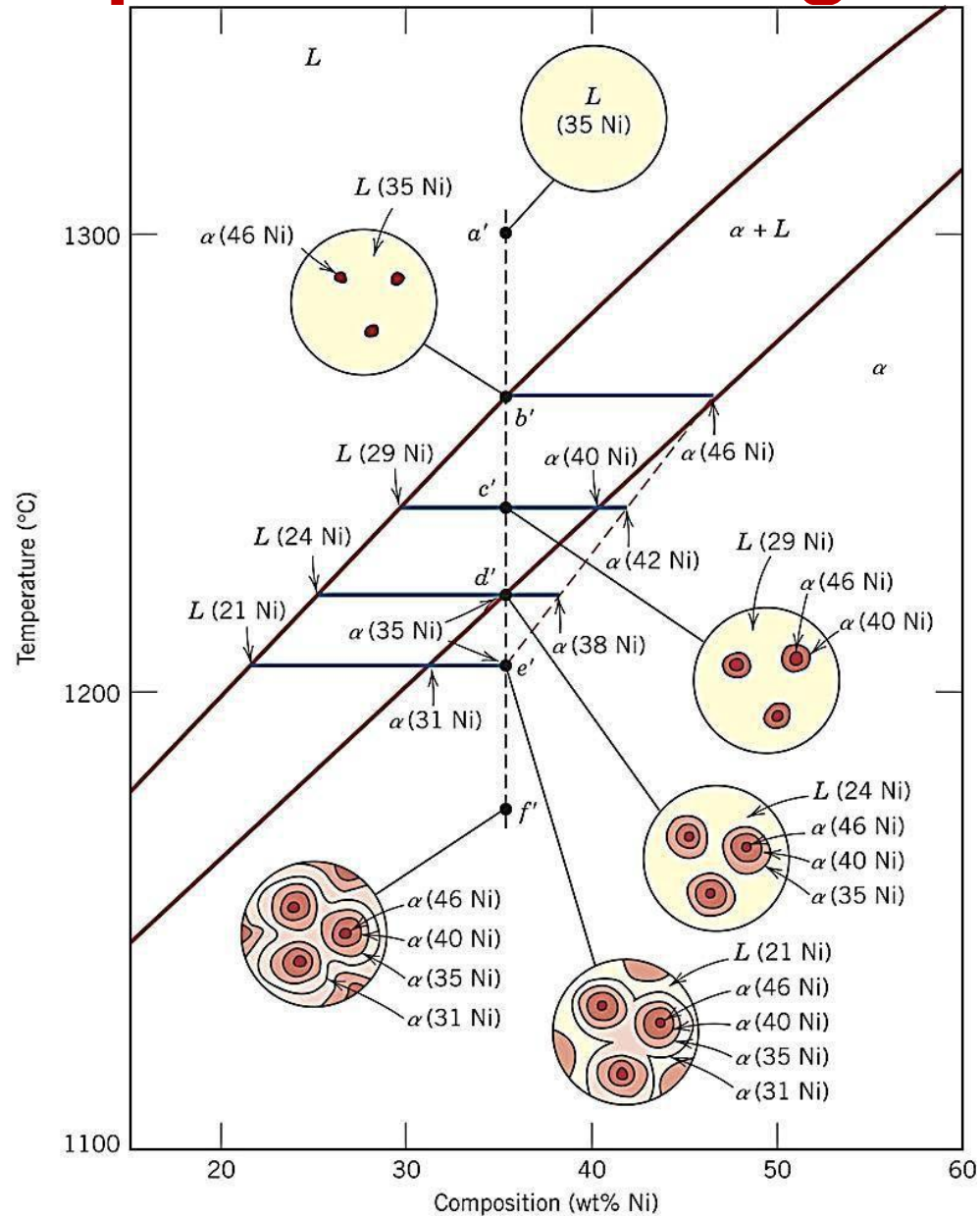
- (between the liquidus and solidus lines): With continued slow cooling, both compositions and relative amounts of each of the phases will change.
- The compositions of the liquid and  $\alpha$ -phases will follow the liquidus and solidus lines, respectively.
- Furthermore, the fraction of the  $\alpha$ -phase will increase with continued cooling.
- The overall alloy composition remains unchanged
- The final product (upon crossing the solidus line) has a uniform composition in a polycrystalline  $\alpha$ -phase solid solution.
- Subsequent cooling will produce no microstructural or composition changes.

# Nonequilibrium Cooling

- Slow cooling: readjustment in the compositions of the liquid and solid phases with changes in temperatures
  - Diffusion in both solid and liquid phases and also across the solid-liquid interface.
  - Diffusion is a time-dependent phenomenon
- In virtually all practical solidification situations, cooling rates are much too rapid to allow these compositional readjustments and maintenance of equilibrium.

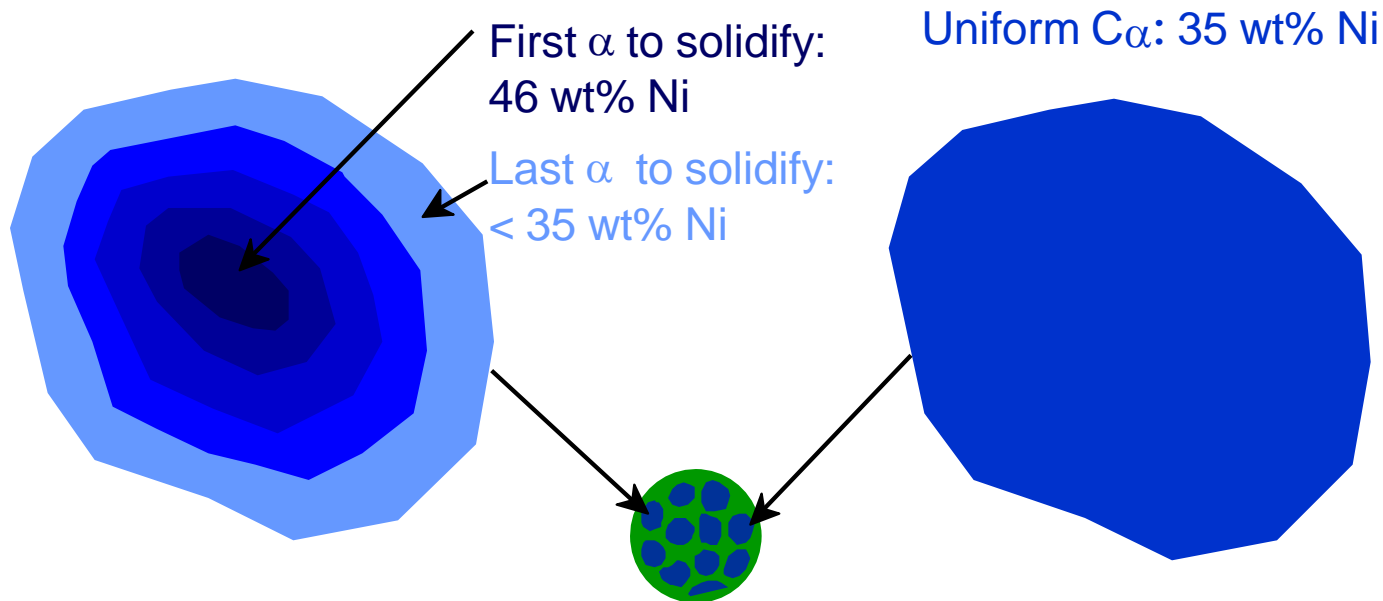
# Nonequilibrium Cooling

- The average composition of the solid  $\alpha$ -grains that have formed would be some volume weighted average composition.
- As a result, the distribution of the two elements within the grains is nonuniform: **Segregation**
- Segregation: concentration gradients are established across the grains.
- **Cored Structure:** the centre of each grain, which is the first part to freeze, is rich in the high-melting element.



# Cored vs Equilibrium Phases

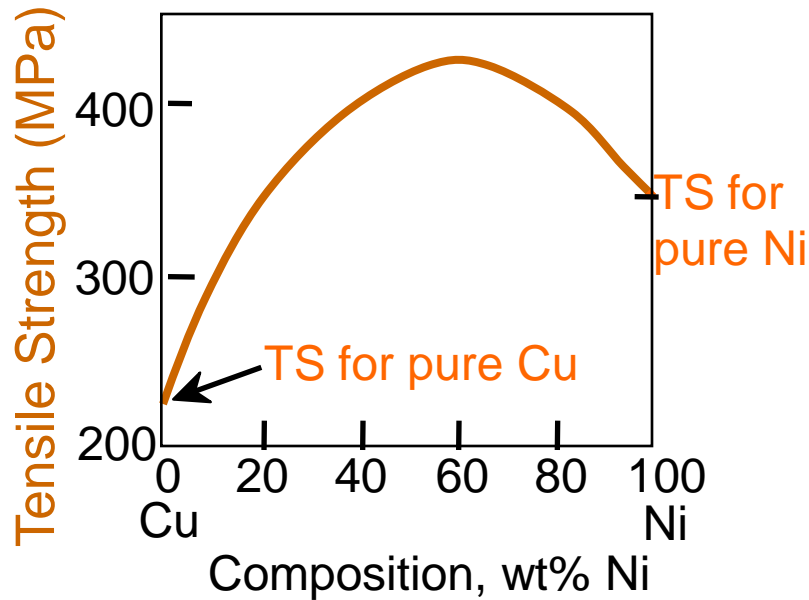
- $C_{\alpha}$  changes as we solidify.
- Cu-Ni case: First  $\alpha$  to solidify has  $C_{\alpha} = 46$  wt% Ni.  
Last  $\alpha$  to solidify has  $C_{\alpha} = 35$  wt% Ni.
- Fast rate of cooling:  
**Cored structure**
- Slow rate of cooling:  
**Equilibrium structure**



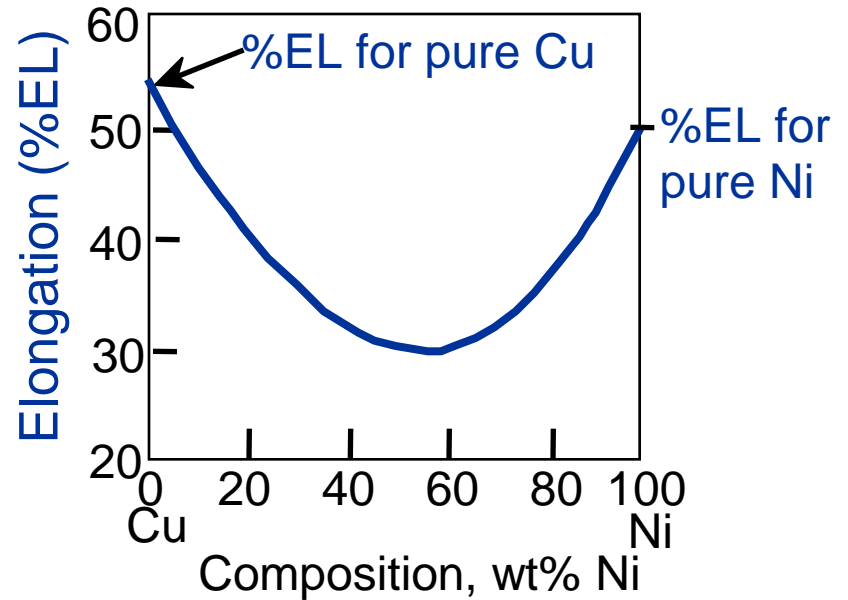
# Mechanical Properties: Cu-Ni System

- Effect of solid solution strengthening on:

-- Tensile strength (TS)

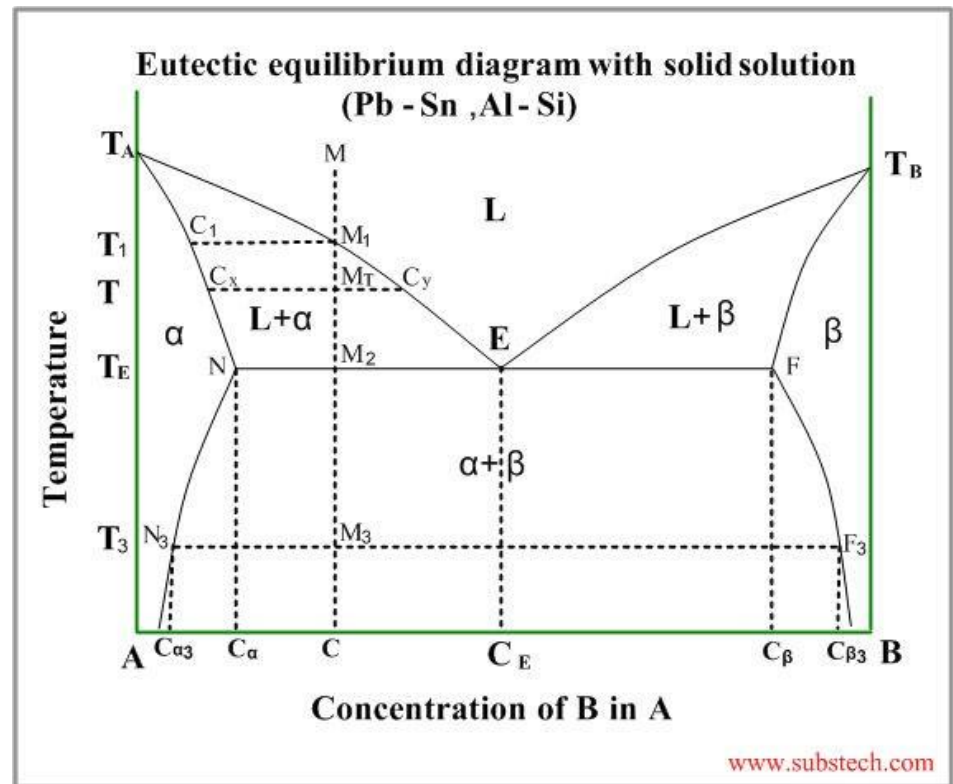


-- Ductility (%EL)



# Eutectic System

A eutectic system is a mixture of chemical compounds or elements that has a single chemical composition that solidifies at a lower temperature than any other composition



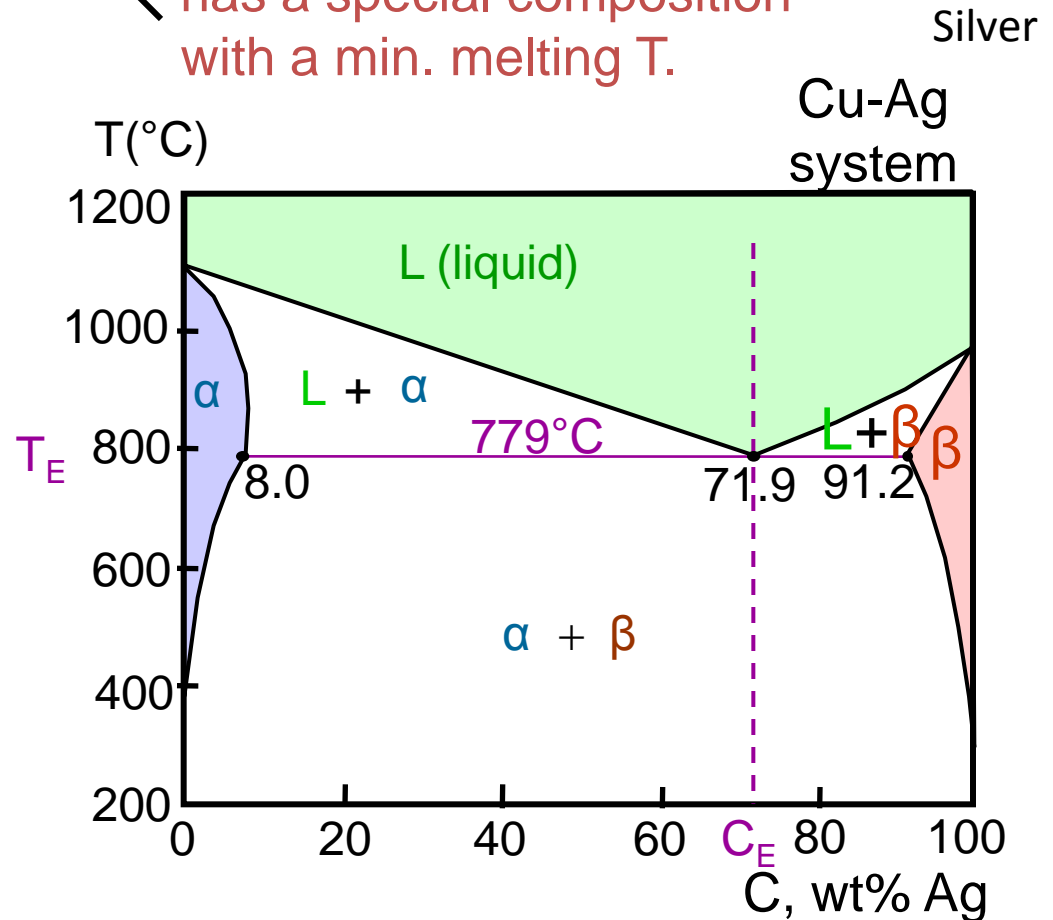
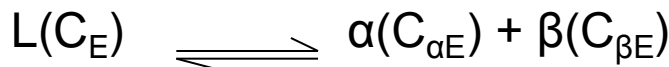
# Binary-Eutectic Systems

2 components

has a special composition with a min. melting T.

Ex.: Cu-Ag system

- 3 single phase regions (L,  $\alpha$ ,  $\beta$ )
- Limited solubility:
  - $\alpha$ : mostly Cu
  - $\beta$ : mostly Ag
- $T_E$ : No liquid below  $T_E$
- $C_E$ : Composition at temperature  $T_E$
- **Eutectic reaction**





# EX 1: Pb-Sn Eutectic System

Lead      Tin

- For a 40 wt% Sn-60 wt% Pb alloy at 150°C, determine:
  - the phases present

**Answer:**  $\alpha + \beta$

- the phase compositions

**Answer:**  $C_\alpha = 11$  wt% Sn  
 $C_\beta = 99$  wt% Sn

- the relative amount of each phase

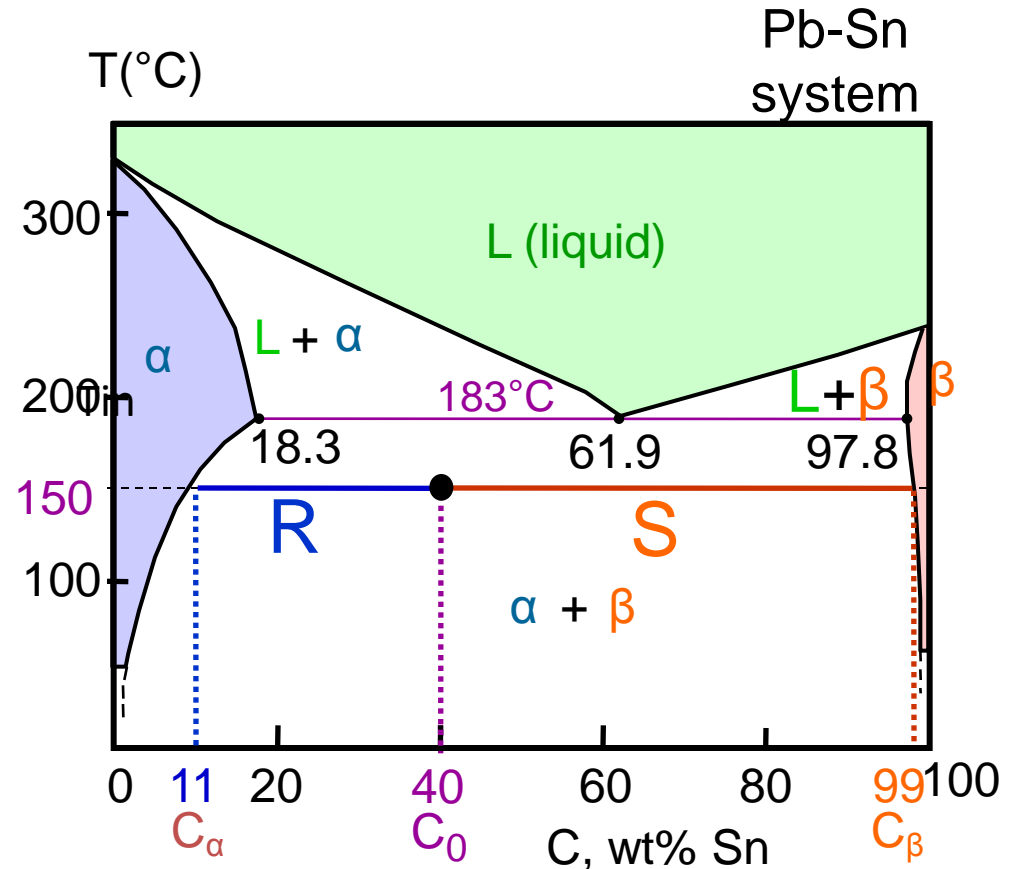
**Answer:**

$$W_\alpha = \frac{S}{R+S} = \frac{C_\beta - C_0}{C_\beta - C_\alpha}$$

$$= \frac{99 - 40}{99 - 11} = \frac{59}{88} = 0.67$$

$$W_\beta = \frac{R}{R+S} = \frac{C_0 - C_\alpha}{C_\beta - C_\alpha}$$

$$= \frac{40 - 11}{99 - 11} = \frac{29}{88} = 0.33$$



# EX 2: Pb-Sn Eutectic System

- For a 40 wt% Sn-60 wt% Pb alloy at 220°C, determine:
  - the phases present:

**Answer:**  $\alpha + L$

- the phase compositions

**Answer:**  $C_\alpha = 17 \text{ wt\% Sn}$   
 $C_L = 46 \text{ wt\% Sn}$

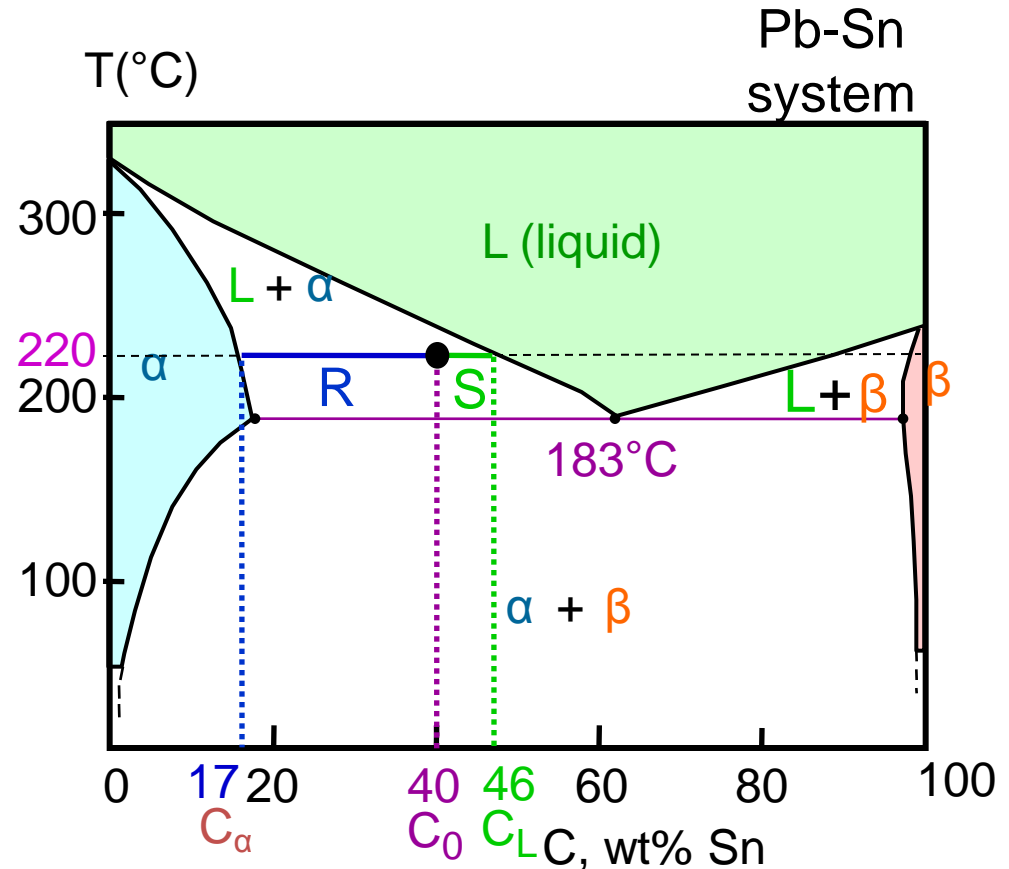
- the relative amount of each phase

**Answer:**

$$W_\alpha = \frac{C_L - C_0}{C_L - C_\alpha} = \frac{46 - 40}{46 - 17}$$

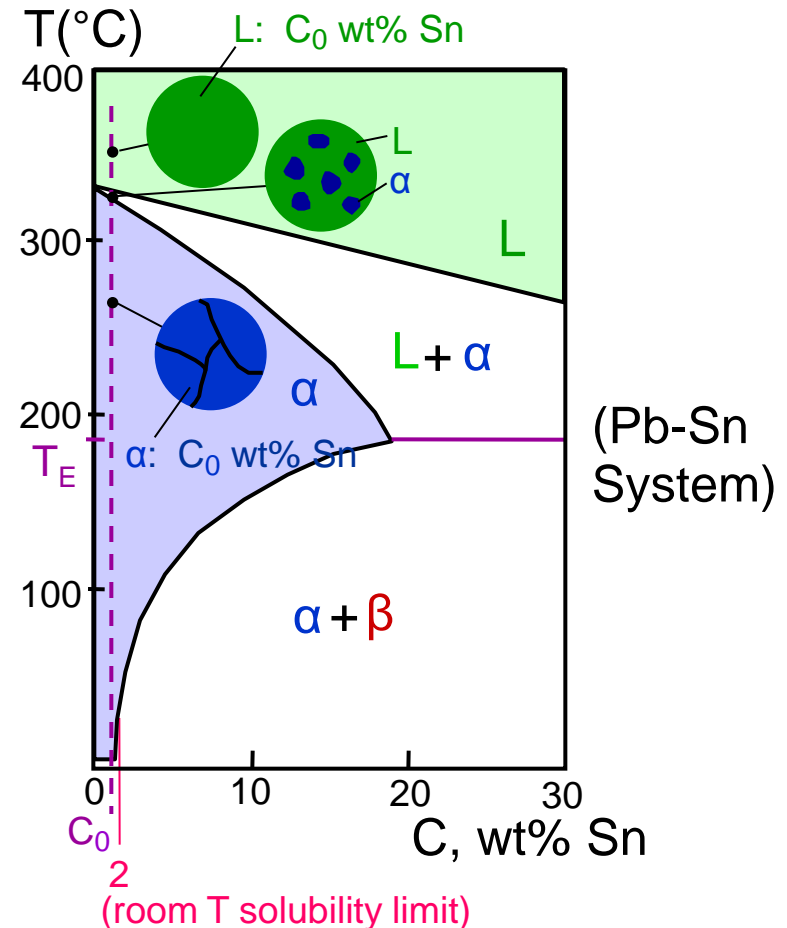
$$= \frac{6}{29} = 0.21$$

$$W_L = \frac{C_0 - C_\alpha}{C_L - C_\alpha} = \frac{23}{29} = 0.79$$



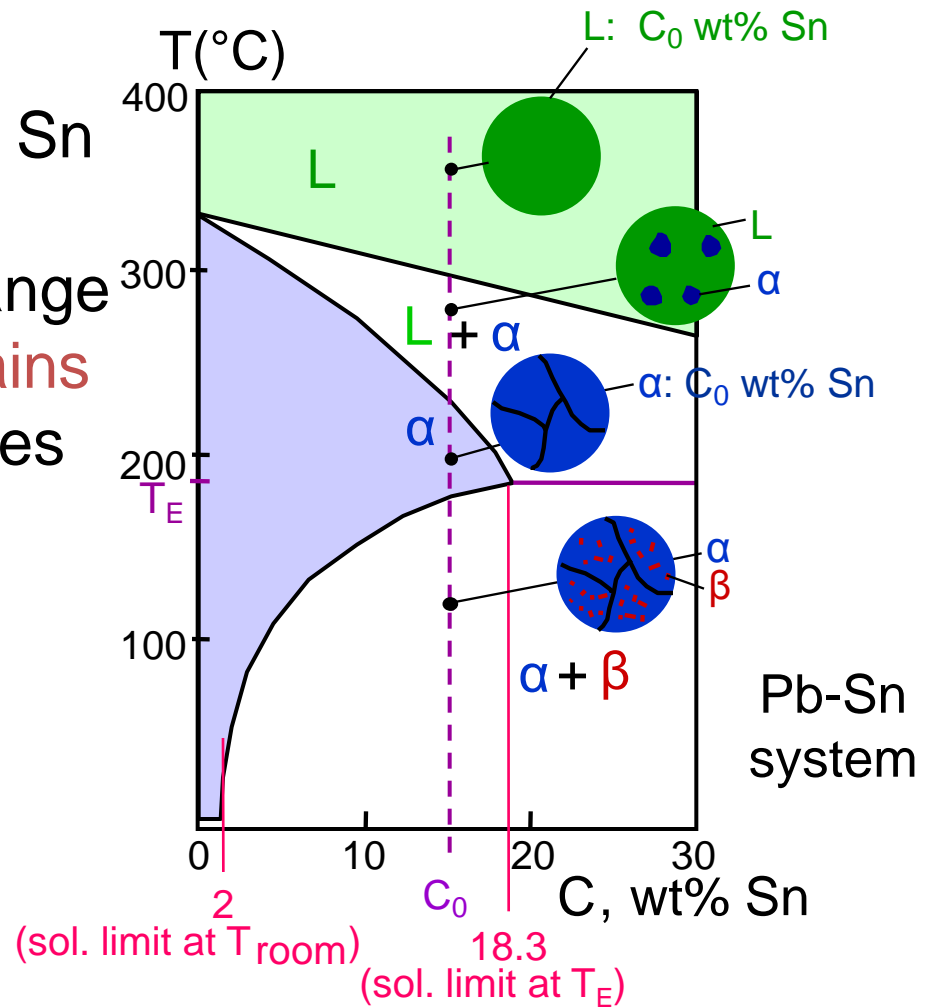
# Microstructural Developments in Eutectic Systems I

- For alloys for which  $C_0 < 2 \text{ wt\% Sn}$
- Result: at room temperature -- polycrystalline with grains of  $\alpha$  phase having composition  $C_0$



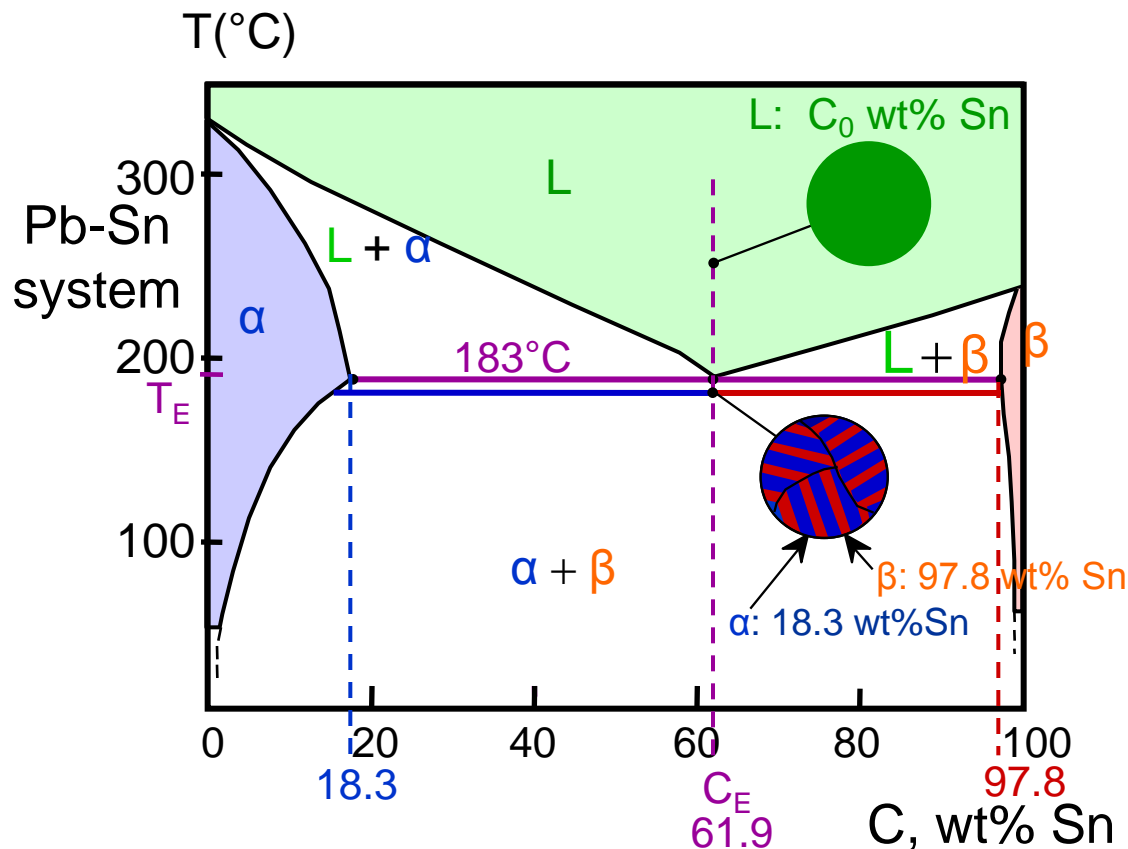
# Microstructural Developments in Eutectic Systems II

- For alloys for which  $2 \text{ wt\% Sn} < C_0 < 18.3 \text{ wt\% Sn}$
- Result: at temperatures in  $\alpha + \beta$  range -- polycrystalline with  $\alpha$  grains and small  $\beta$ -phase particles



# Microstructural Developments in Eutectic Systems III

- For alloy of composition  $C_0 = C_E$
- Result: Eutectic microstructure (lamellar structure)
  - alternating layers (lamellae) of  $\alpha$  and  $\beta$  phases.



Micrograph of Pb-Sn  
eutectic  
microstructure

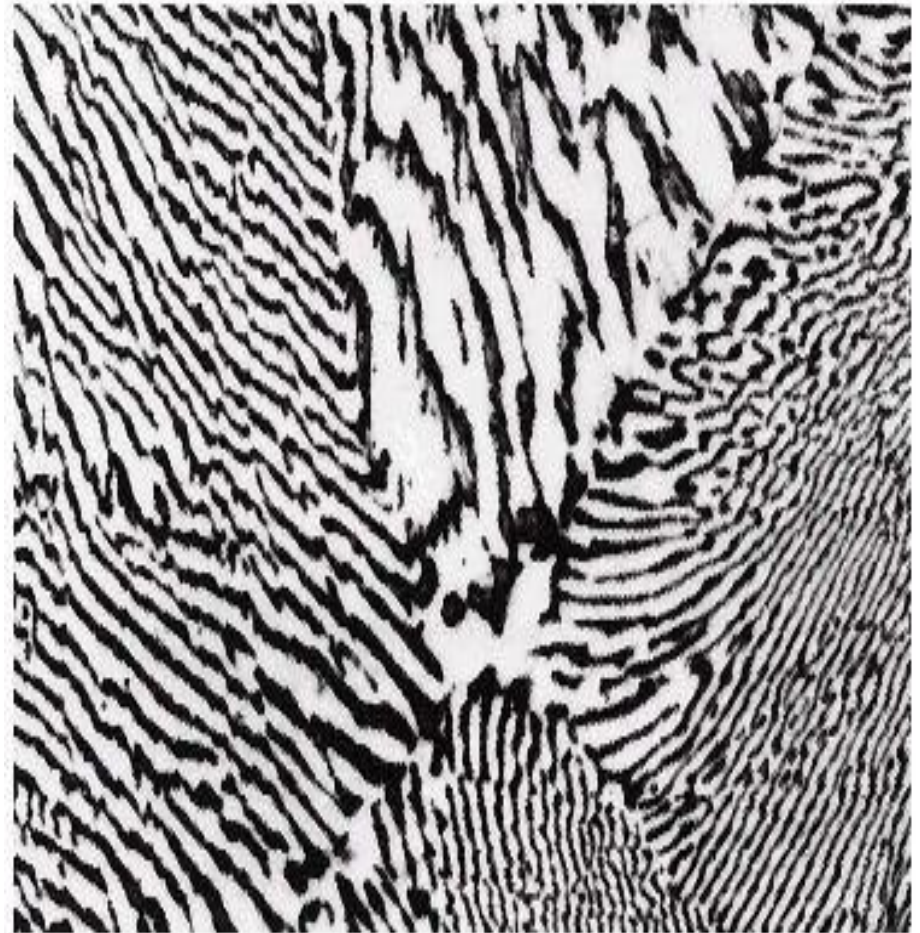
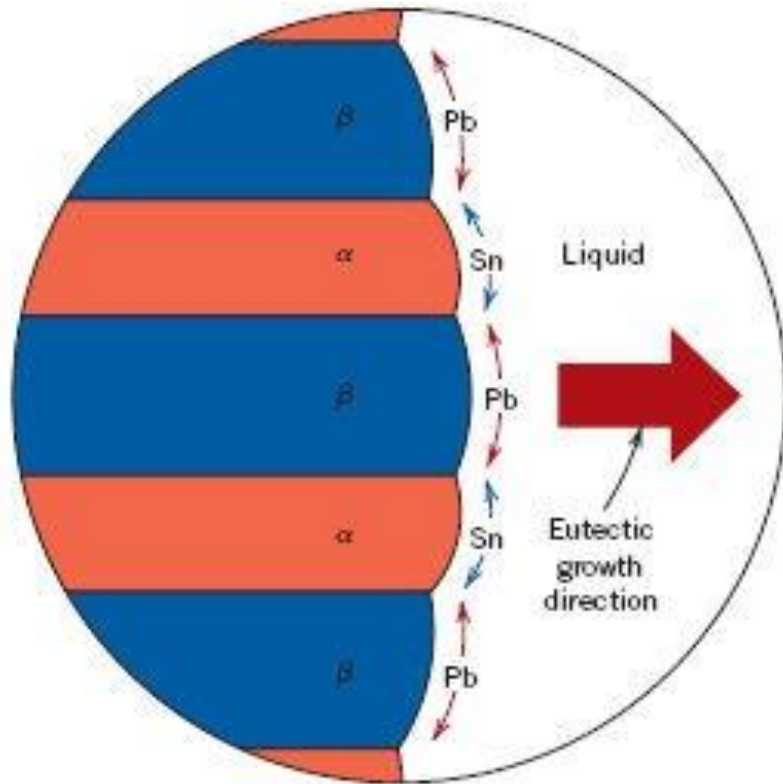


160  $\mu\text{m}$

# Microstructural Developments in Eutectic Systems III

- The microstructure of the solid results from the Eutectic transformation consists of alternating layers (called lamellae) of the  $\alpha$  and  $\beta$  phases that form simultaneously during the transformation.
- The microstructure at Eutectic point is called **EUTECTIC STRUCTURE.**
- Subsequent cooling of the alloy form just below the eutectic to room temperature will result in only minor microstructural alterations.

# Lamellar Eutectic Structure



# Microstructural Developments in Eutectic Systems III

- The  $\alpha$ - $\beta$  layered eutectic growing into and replacing the liquid phase
- The process of redistribution of lead and tin occurs by diffusion in the liquid just ahead of the eutectic-liquid interface.
- The arrows indicate the directions of diffusion of lead and tin atoms; lead atoms diffuse toward the  $\alpha$ -phase layers because this  $\alpha$ -phase is lead-rich.
- Similarly for the tin-rich phase

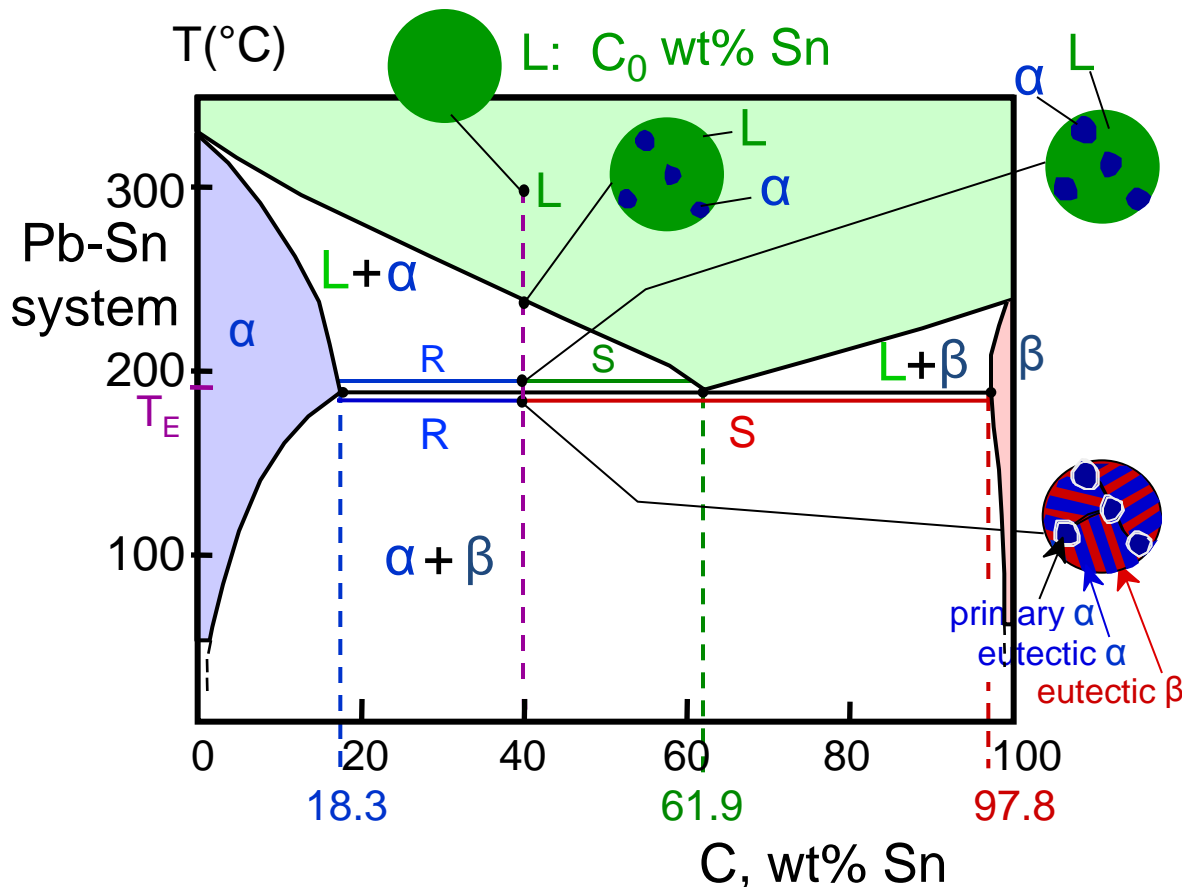


# 60/40 TIN-LEAD SOLDER

- A familiar example is the 60/40 solder, a low-melting temperature having near-Eutectic compositions.
- An alloy of this composition is completely molten about 185 C, which makes it especially attractive as a low- temperature solder.

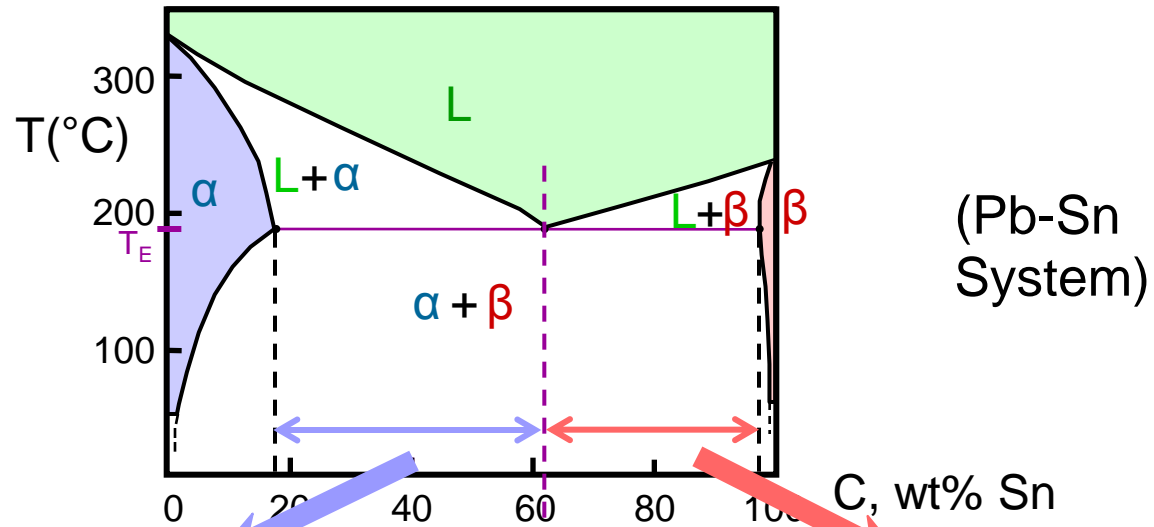
# Microstructures in Eutectic Systems (Pb-Sn): IV

- For alloys for which  $18.3 \text{ wt\% Sn} < C_0 < 61.9 \text{ wt\% Sn}$
- Result:  $\alpha$  phase particles and a eutectic microstructure

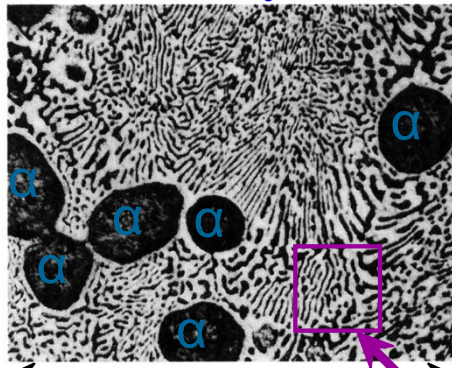


- Just above  $T_E$  :
  - $C_\alpha = 18.3 \text{ wt\% Sn}$
  - $C_L = 61.9 \text{ wt\% Sn}$
  - $W_\alpha = \frac{S}{R+S} = 0.50$
  - $W_L = (1 - W_\alpha) = 0.50$
- Just below  $T_E$  :
  - $C_\alpha = 18.3 \text{ wt\% Sn}$
  - $C_\beta = 97.8 \text{ wt\% Sn}$
  - $W_\alpha = \frac{S}{R+S} = 0.73$
  - $W_\beta = 0.27$

# Hypoeutectic & Hypereutectic



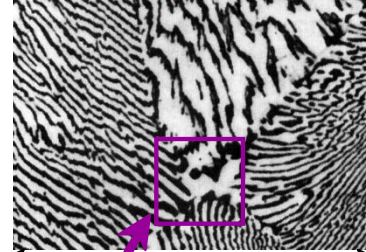
hypoeutectic:  $C_0 = 50 \text{ wt\% Sn}$



175  $\mu\text{m}$

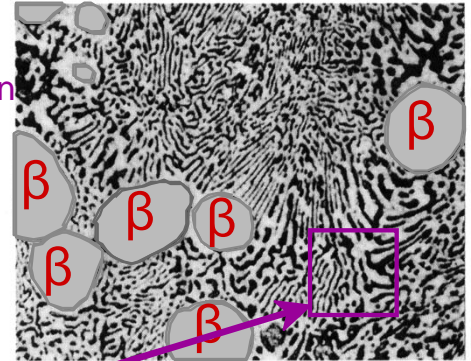
eutectic  
61.9

eutectic:  $C_0 = 61.9 \text{ wt\% Sn}$



160  $\mu\text{m}$

hypereutectic: (illustration only)



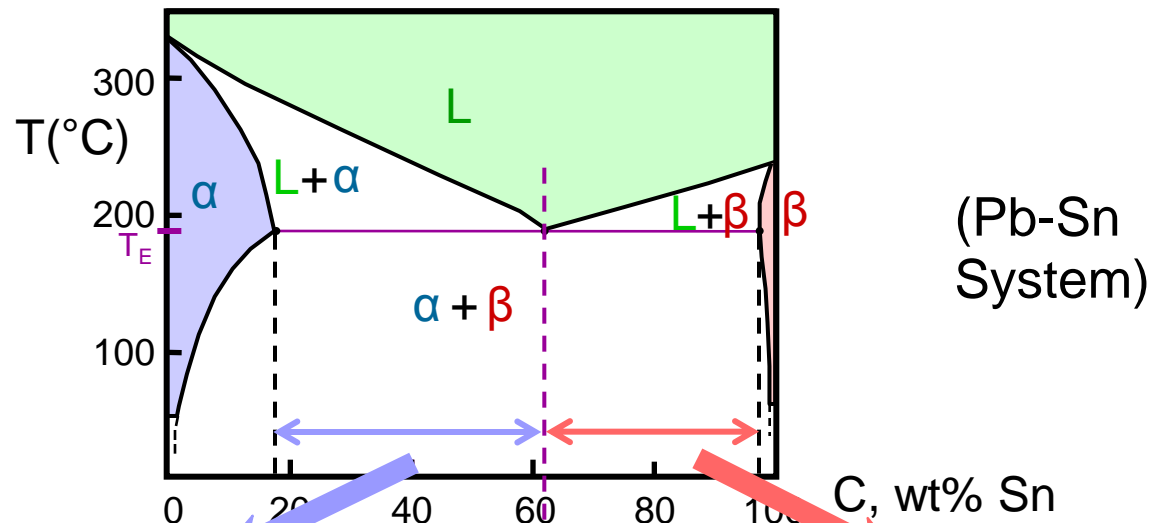
160  $\mu\text{m}$

eutectic micro-constituent

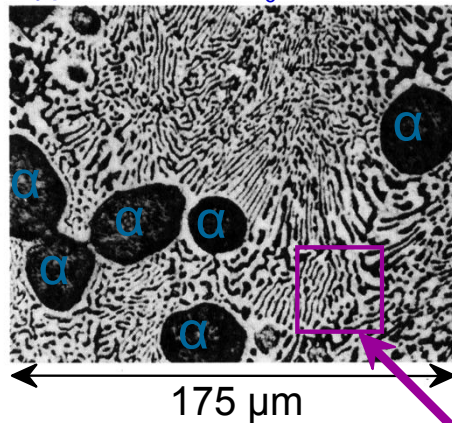
# Microstructural Developments in Eutectic Systems IV

- Insignificant changes will occur with the phase that formed during cooling through the  $\alpha + L$  region.
- So the  $\beta$ -phase will be present in the eutectic structure and also as the phase that formed while cooling through the  $\alpha + L$  phase field.
- So there are two **microconstituents**:  $\alpha$  and eutectic structures.
- **Microconstituent is an element of the microstructure having an identifiable and characteristic structure.**
- It is possible to compute the relative amounts of both eutectic and primary microconstituents.

# Hypoeutectic & Hypereutectic

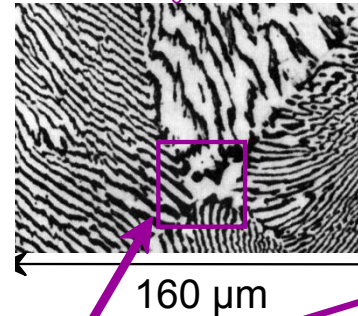


hypoeutectic:  $C_0 = 50 \text{ wt\% Sn}$

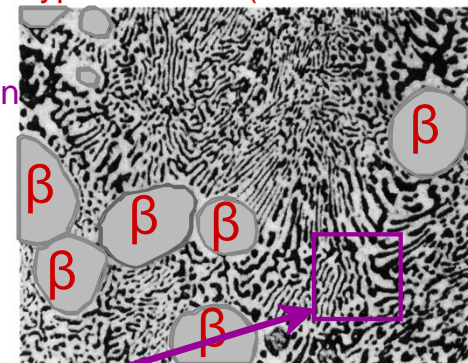


eutectic  
61.9

eutectic:  $C_0 = 61.9 \text{ wt\% Sn}$



hypereutectic: (illustration only)



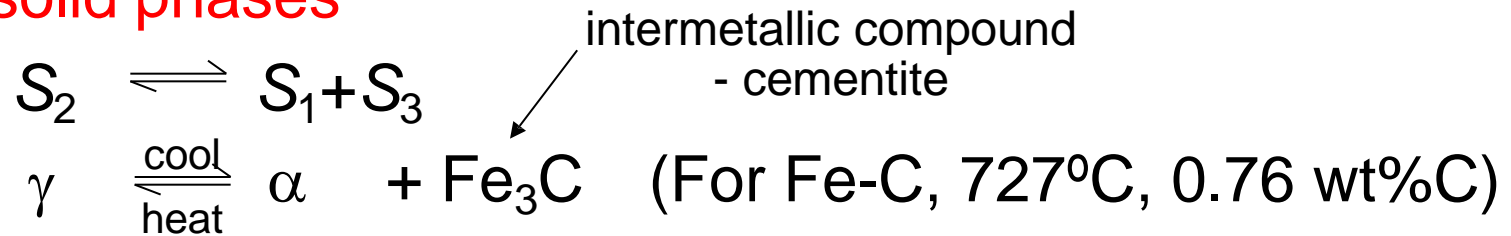
eutectic micro-constituent

# Eutectic, Eutectoid, & Peritectic

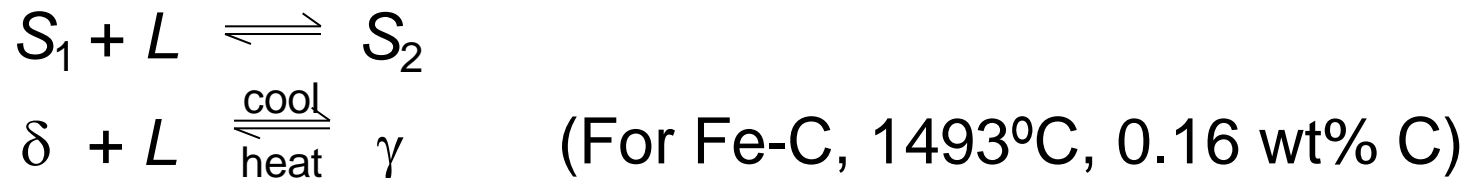
- **Eutectic** - liquid transforms to two solid phases



- **Eutectoid** – one solid phase transforms to two other solid phases



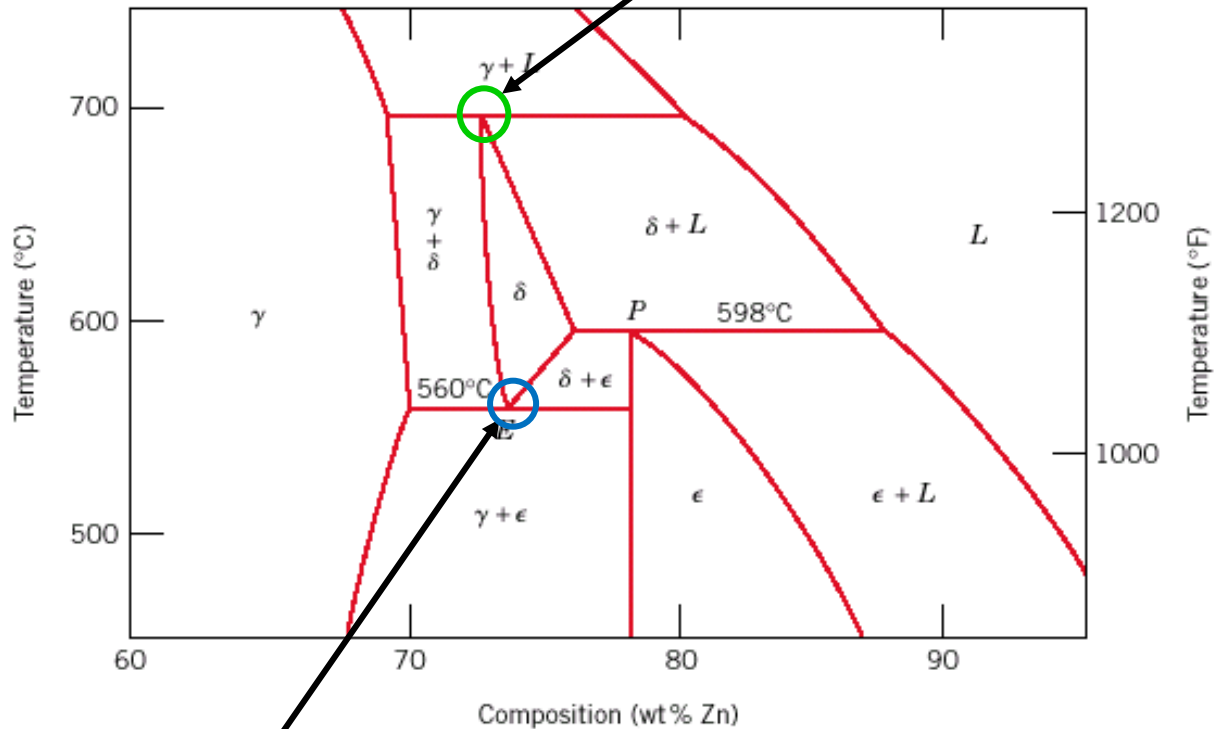
- **Peritectic** - liquid and one solid phase transform to a second solid phase



# Eutectoid & Peritectic

## Cu-Zn Phase diagram

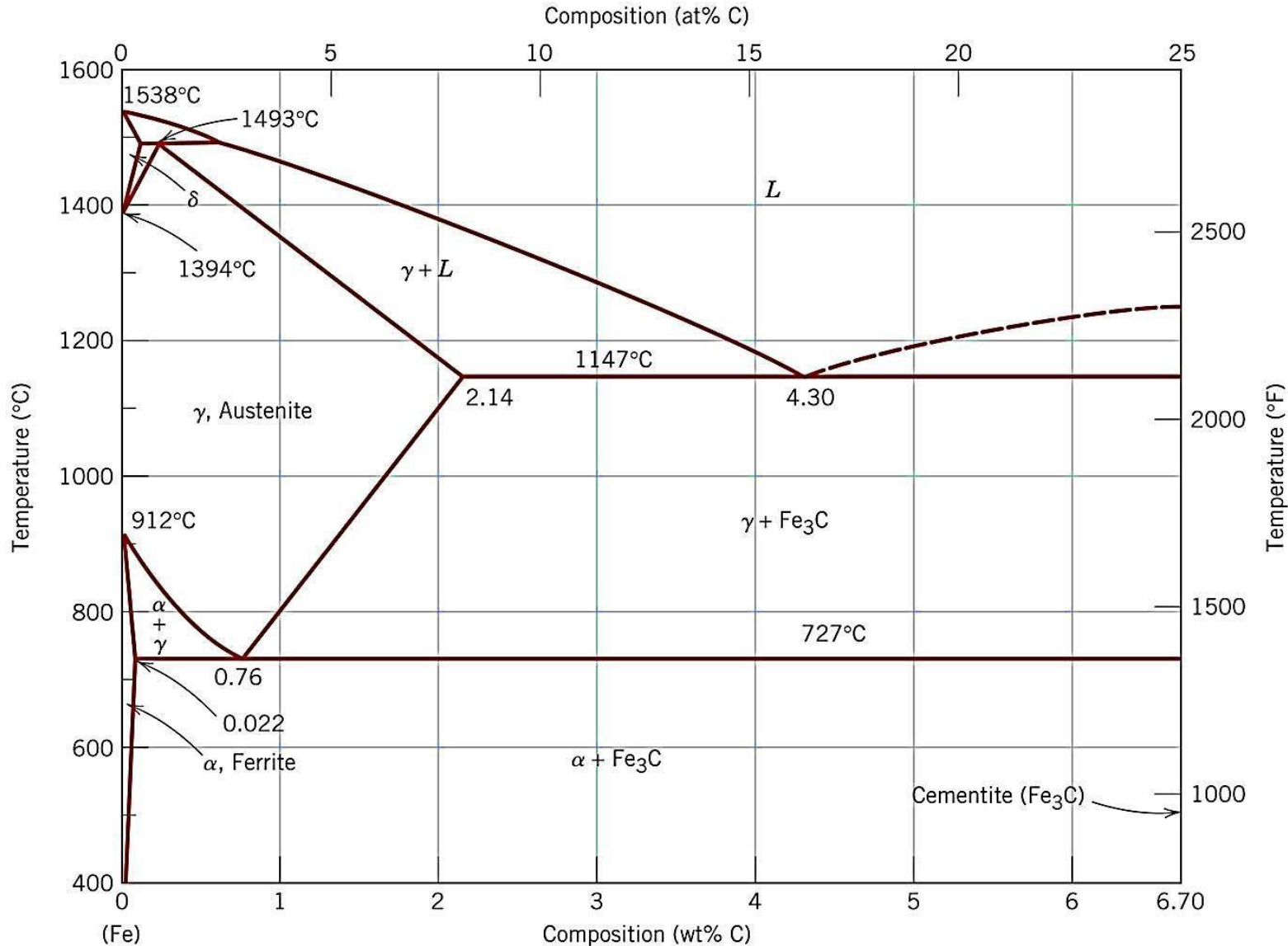
Peritectic transformation  $\gamma + L \rightleftharpoons \delta$



Eutectoid transformation  $\delta \rightleftharpoons \gamma + \epsilon$

# IRON-CARBON (Fe-C) PHASE DIAGRAM

Adapted from  
Fig. 9.24, *Callister  
& Rethwisch 8e.*





# FERRITE

- **Ferrite** or  $\alpha$ -iron has a BCC crystal structure.
- Only a small concentrations of carbon are soluble in  $\alpha$ -ferrite (0.022 wt% at 727 °C).
- Carbon significantly influences the mechanical properties of ferrite even at small concentrations of carbon
- This particular iron-carbon phase is relatively soft, may be magnetic at temperatures below 768 °C

# AUSTENITE

- At 912 °C, ferrite experiences a polymorphic transformation to FCC **austenite** (or  $\gamma$ -iron).
- $\gamma$ -phase of iron alloyed with carbon is not stable below 727 °C.
- The maximum solubility of carbon in austenite is 2.14 wt%, occurs at 1147 °C.
- This solubility is approximately 100 times greater than the maximum for BCC ferrite, because the FCC interstitial positions are larger.
- Austenite is nonmagnetic.

# $\delta$ -FERRITE

- At 1394 °C, the austenite reverts back to a BCC phase known as  $\delta$ -ferrite, which finally melts at 1538 °C.
- $\delta$ -ferrite is virtually the same as  $\alpha$ -ferrite, except for the range of temperatures over which each exists.
- Because  $\delta$ -ferrite is stable only at relatively high temperatures, it will not be discussed further.

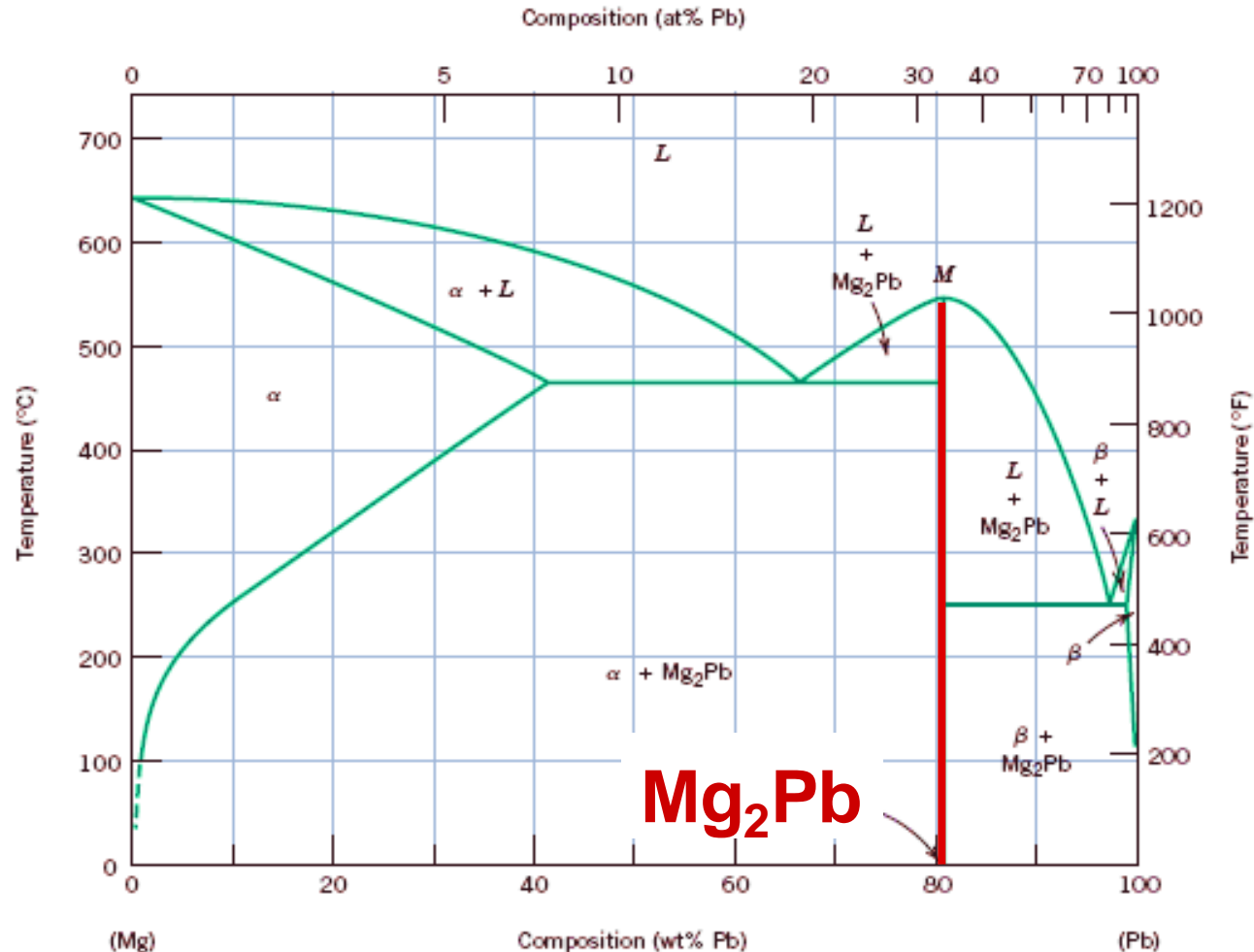
# CEMENTITE

- The composition axis in Figure (Fe- Fe<sub>3</sub>C phase diagram) extends only to 6.70 wt% C: the intermediate compound iron carbide or **cementite** (Fe<sub>3</sub>C): represented by a vertical line on the phase diagram.
- In practice, all steels and cast irons have carbon contents less than 6.7 wt% C.
- Cementite forms when the solubility limit of carbon in  $\alpha$ -ferrite is exceeded below 727 °C ( $\alpha$  coexists with Fe<sub>3</sub>C).
- Fe<sub>3</sub>C also coexists with  $\gamma$ -phase between 727 and 1147 °C.
- Cementite is very hard and brittle.

# FERROUS ALLOYS

- Are those in which iron is the prime component, but carbon as well as other alloying elements may be present.
- Three classification of ferrous alloys based on carbon content: iron, steel, and cast iron.
- Commercially, pure iron contains less than 0.008 wt% (almost exclusively  $\alpha$  -phase at room temperature).
- Iron-carbon alloys that contain 0.008-2.14 wt% C are classified as steels (mostly  $\alpha + \text{Fe}_3\text{C}$ )
- Cast iron contain 2.14-6.70 wt% C (commercially less than 4.5 wt%)

# Intermetallic Compounds



Adapted from  
Fig. 9.20, Callister &  
Rethwisch 8e.

Note: intermetallic compound exists as a line on the diagram - not an area - because of stoichiometry (i.e. composition of a compound is a fixed value).

# Intermetallic Compounds

- That means that **Mg<sub>2</sub>Pb** can exist by itself only at the precise composition of 19 wt% Mg-81 wt% Pb.
- In other words, discrete intermediate compounds rather than solid solutions may be found on the phase diagram.
- These compounds have distinct chemical formulas; for metal-metal systems (**intermetallic compounds**).

# OTHER CHARACTERISTICS OF Mg-Pb SYSTEM

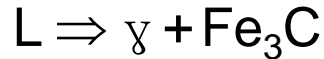
- $\text{Mg}_2\text{Pb}$  melts at approximately 550 °C.
- The solubility of lead in magnesium is rather extensive.
- The solubility of magnesium in lead is extremely limited.
- There are two eutectic reactions.



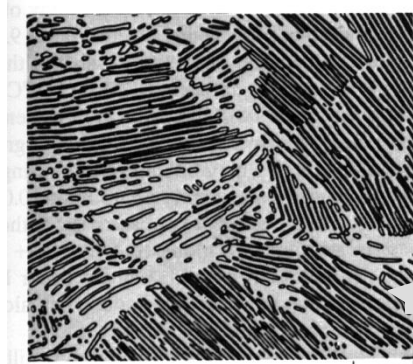
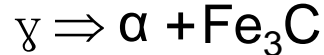
# Iron-Carbon (Fe-C) Phase Diagram

- 2 important points

- Eutectic (A):



- Eutectoid (B):



Result: Pearlite = alternating layers of  $\alpha$  and  $\text{Fe}_3\text{C}$  phases

