

# The Limitation of Equilibrium Phase Diagrams

- Unable to indicate the **time** period required for the attainment of equilibrium
- **Equilibrium conditions** are maintained only if heating or cooling is carried out at extremely slow and unpractical rates.

# Chapter 10: Phase Transformations

## WHY STUDY PHASE TRANSFORMATION?

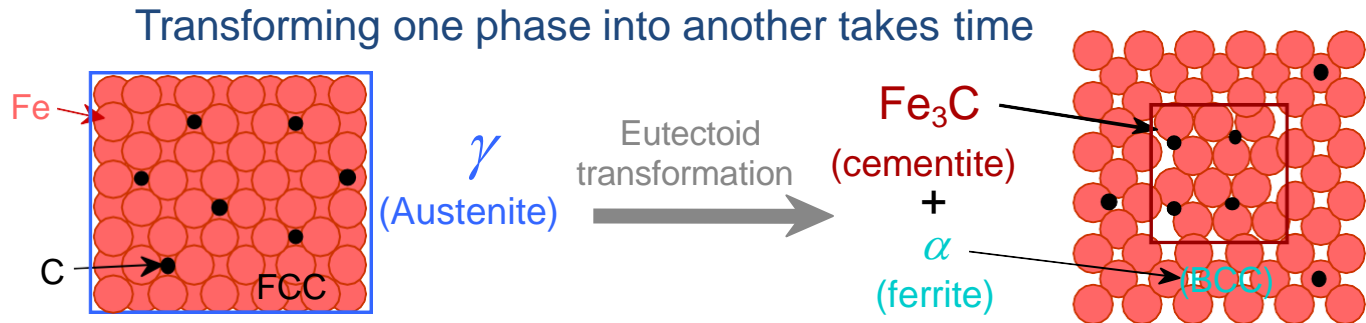
- The development of a set of desirable mechanical characteristics for a material often results from a phase transformation. That is wrought by **heat-treatment**.
- It is important to design a proper heat-treatment to get the desired room-temperature mechanical properties of an alloy.
- **Is it possible to develop other microstructural elements than pearlite for iron-carbon alloys?**

# Phase Transformations

- Phase transformation may be wrought in metal alloy systems by varying temperature, composition, and the external pressure.
- Temperature changes by means of heat-treatments are most conveniently utilized to induce phase transformations.
- This corresponds to crossing a phase boundary on the composition-temperature phase diagram as an alloy of a given temperature is heated or cooled.
- One limitation of phase diagrams is their inability to indicate the time period required for the attainment of equilibrium.
- Equilibrium conditions are maintained only if heating or cooling is carried out at extremely slow and unpractical rates.

# THE INFLUENCE OF TIME

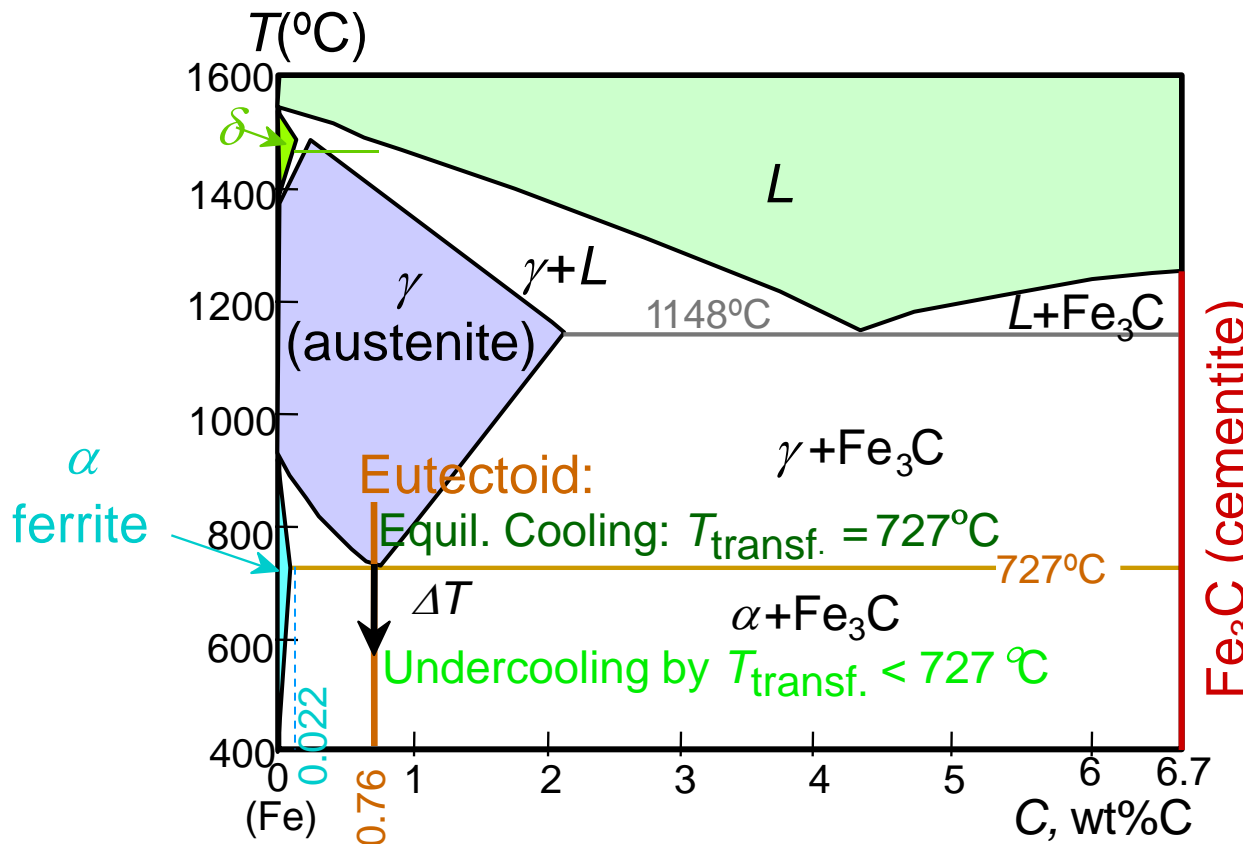
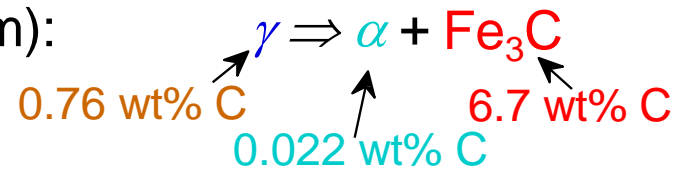
- Why it is important to study the influence of time on phase transformation?
- How does the rate of transformation depend on time and temperature?



- For other than equilibrium cooling, transformations are shifted to lower temperatures than indicated by the phase diagram.
- **Supercooling:** the shift to lower temperatures for cooling
- **Superheating:** the shift to higher temperatures for heating

# Transformations & Undercooling

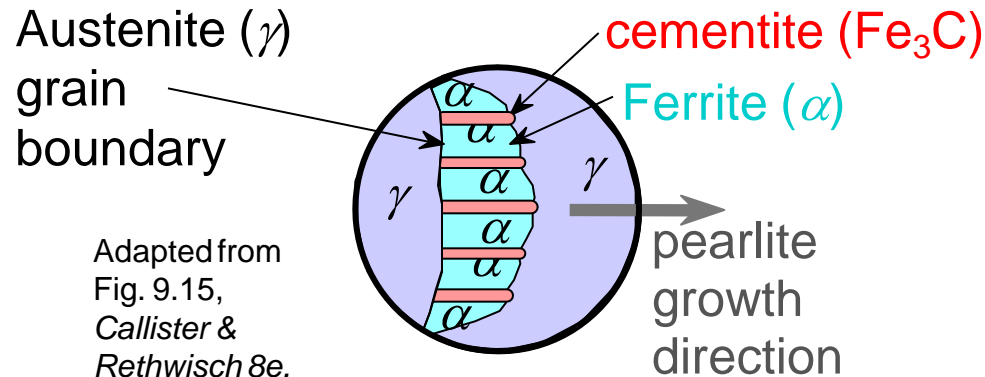
- Eutectoid transf. (Fe-Fe<sub>3</sub>C system):
- For transf. to occur, must cool to below 727°C (i.e., must “undercool”)



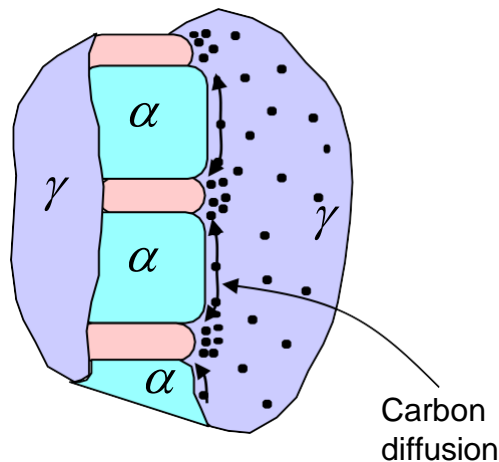
Adapted from Fig. 9.24, Callister & Rethwisch 8e. (Fig. 9.24 adapted from *Binary Alloy Phase Diagrams*, 2nd ed., Vol. 1, T.B. Massalski (Ed.-in-Chief), ASM International, Materials Park, OH, 1990.)

# The Fe-Fe<sub>3</sub>C Eutectoid Transformation

- Transformation of austenite to pearlite:



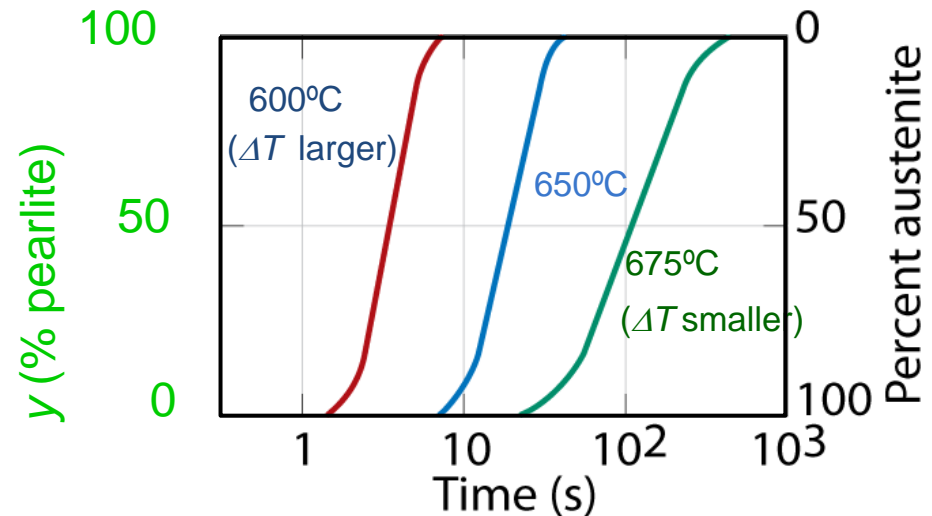
Diffusion of C during transformation



# The Fe-Fe<sub>3</sub>C Eutectoid Transformation (cont.)

- For this transformation, rate increases with  $[T_{\text{eutectoid}} - T]$  (i.e.,  $\Delta T$ ).

Adapted from Fig. 10.12, Callister & Rethwisch 8e.



- S-shaped curves of the percentage transformation versus the logarithm of time at three different temperatures.
- For each curve, data were collected after rapidly cooling a specimen composed of 100% austenite to the temperature indicated.
- That temperature was maintained constant throughout the course of the reaction.

# ISOTHERMAL TRANSFORMATION DIAGRAMS

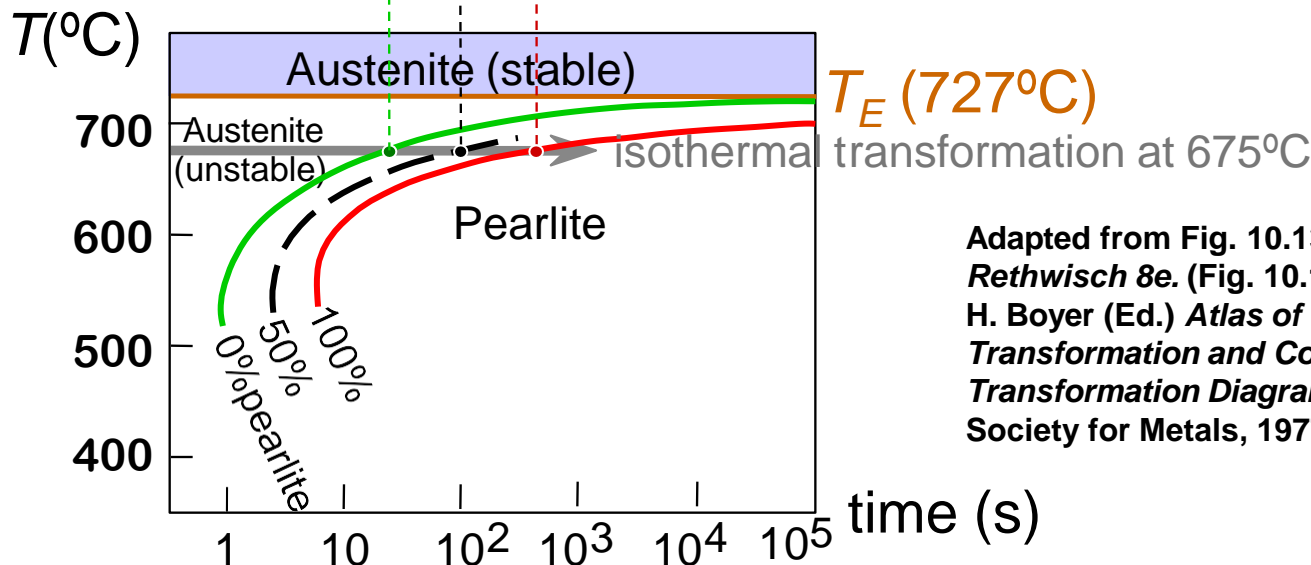
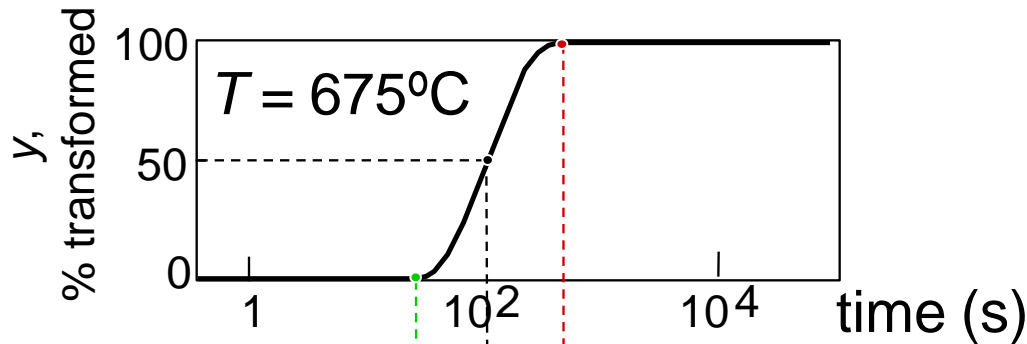
- A more convenient way of representing both the time and temperature dependence of this transformation.
- These curves were generated from a series of plots of the percentage transformations versus the logarithm of time taken over a range of temperatures (from the S-shaped curves).



# Generation of Isothermal Transformation Diagrams

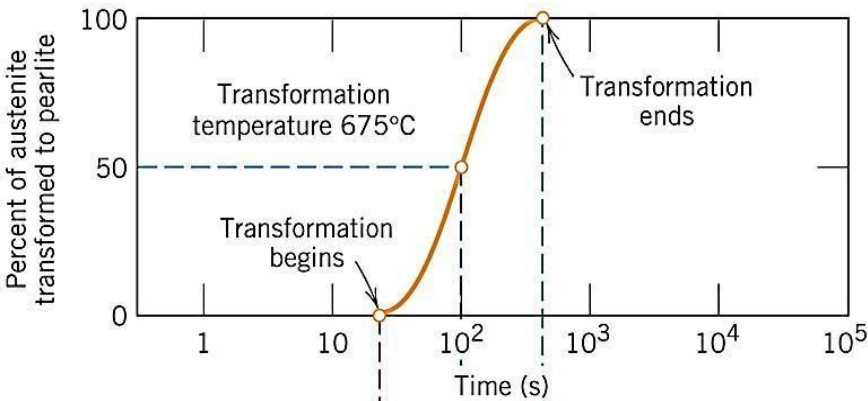
Consider:

- The Fe-Fe<sub>3</sub>C system, for  $C_0 = 0.76$  wt% C
- A transformation temperature of 675°C.



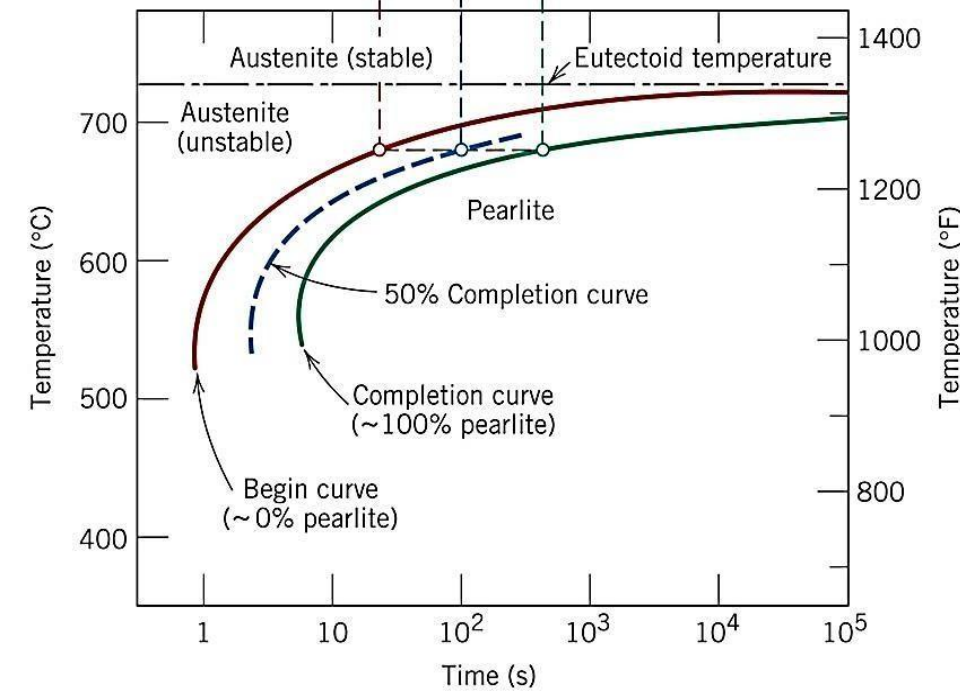
Adapted from Fig. 10.13, *Callister & Rethwisch 8e*. (Fig. 10.13 adapted from H. Boyer (Ed.) *Atlas of Isothermal Transformation and Cooling Transformation Diagrams*, American Society for Metals, 1977, p. 369.)

# Generation of Isothermal Transformation Diagrams



Consider:

- The Fe-Fe<sub>3</sub>C system, for  $C_0 = 0.76 \text{ wt\% C}$
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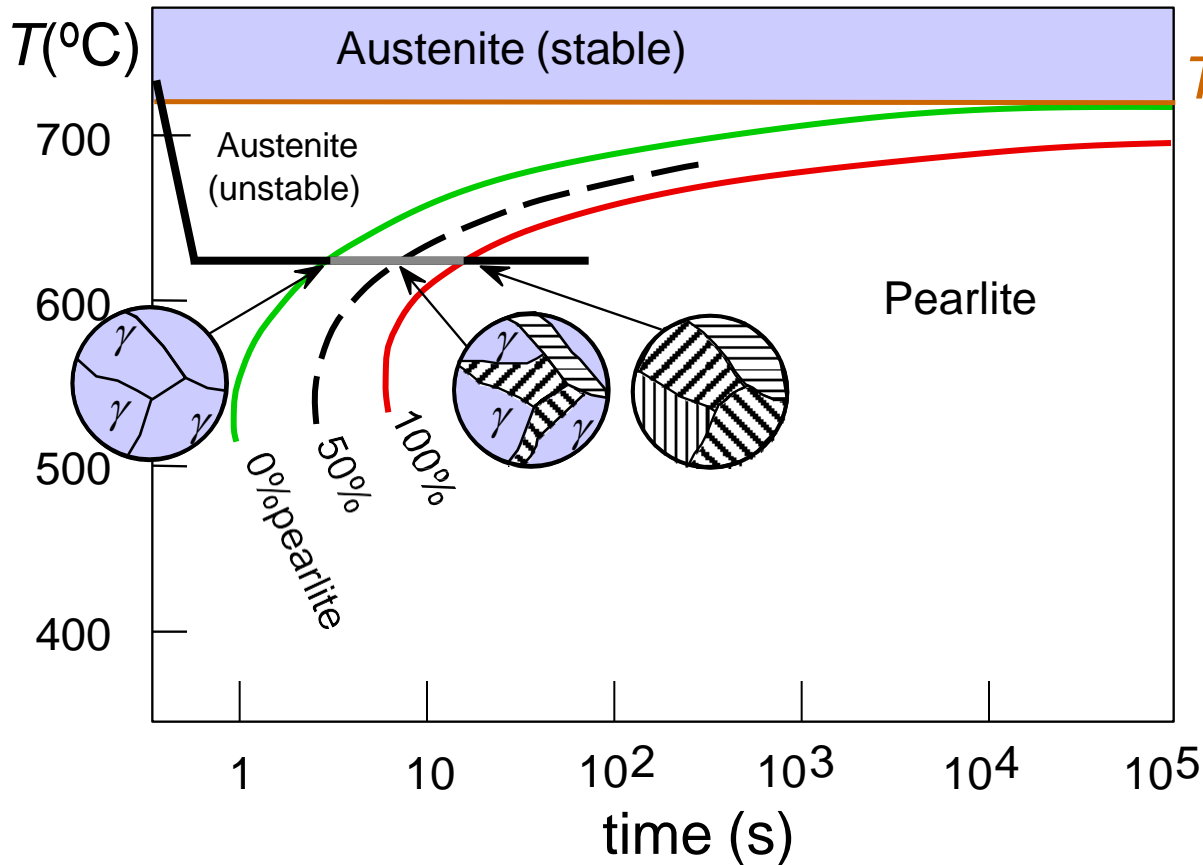
Adapted from Fig. 10.13, *Callister & Rethwisch 8e*. (Fig. 10.13 adapted from H. Boyer (Ed.) *Atlas of Isothermal Transformation and Cooling Transformation Diagrams*, American Society for Metals, 1977, p. 369.)

# ISOTHERMAL TRANSFORMATION DIAGRAMS

- The austenite-to-pearlite transformation will occur only if an alloy is supercooled to below the eutectoid
- The time necessary for the transformation to begin and then end depends on temperature.
- The start and finish curves are nearly parallel, and they approach the eutectoid line asymptotically.
- To the left of the transformation start curve, only austenite (unstable) will be present
- To the right of the finish curve, only pearlite will exist.
- In between, the austenite is in the process of transforming to pearlite, and both microconstituents will be present.

# Austenite-to-Pearlite Isothermal Transformation

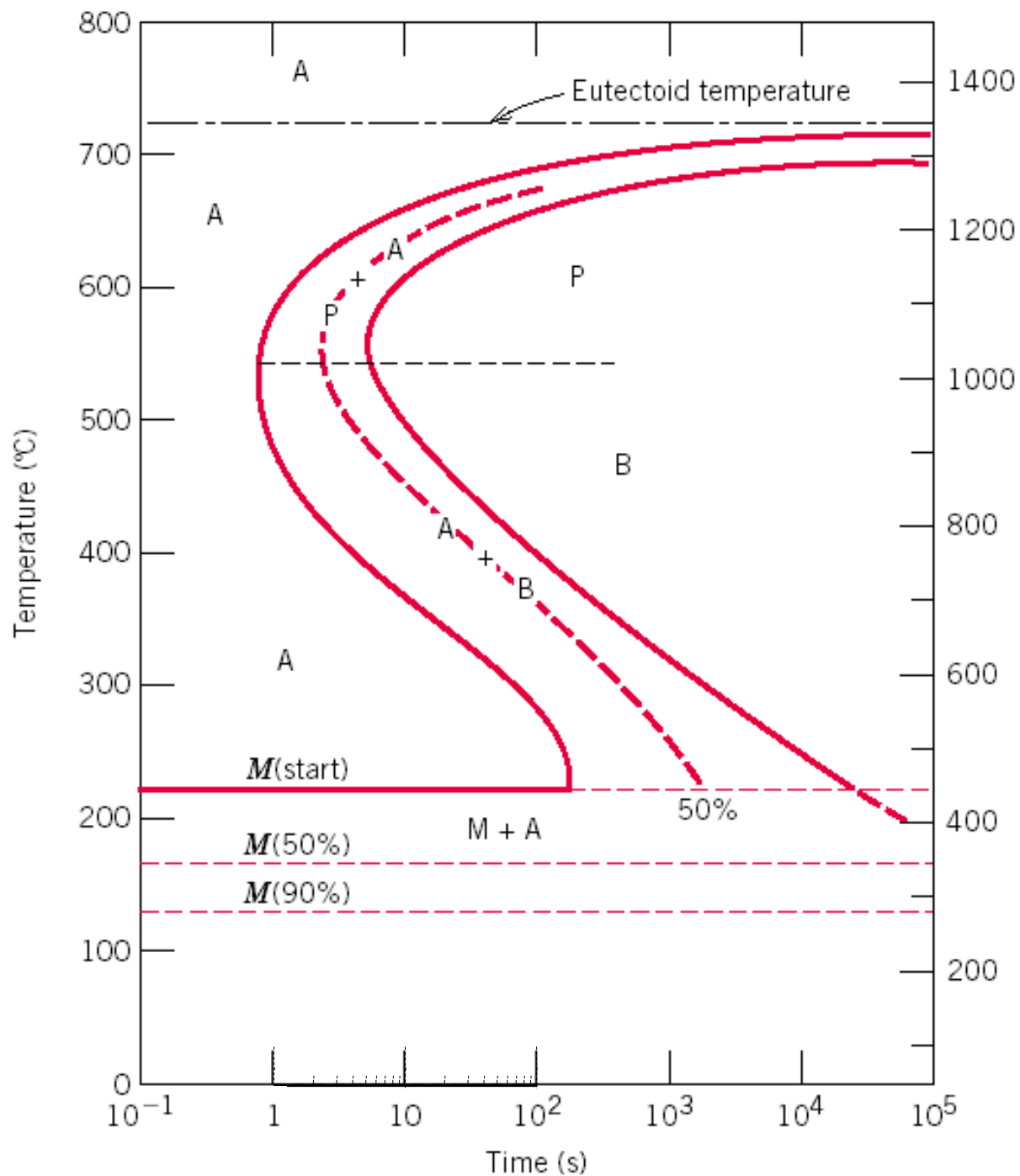
- Eutectoid composition,  $C_0 = 0.76 \text{ wt\% C}$
- Begin at  $T > 727^\circ\text{C}$
- Rapidly cool to  $625^\circ\text{C}$
- Hold  $T$  ( $625^\circ\text{C}$ ) constant (isothermal treatment)



Adapted from Fig. 10.14, Callister & Rethwisch 8e. (Fig. 10.14 adapted from H. Boyer (Ed.) *Atlas of Isothermal Transformation and Cooling Transformation Diagrams*, American Society for Metals, 1997, p. 28.)

# Austenite-to-Pearlite Isothermal Transformation (cont.)

- This plot is only valid for an iron-carbon alloy of eutectoid composition (different curves for other alloys).
- Such a plot is called **isothermal transformation diagram** or **time-temperature-transformation (T-T-T)**.
- Shorter the time → higher is the rate of transformation
- For instance, at temperatures just below the eutectoid, very long times are required for the 50% transformation (i.e., the action rate is very slow).
- Coarse pearlite → formed at higher temperatures – relatively soft
- Fine pearlite → formed at lower temperatures – relatively hard



**The complete TTT diagram for an iron-carbon alloy of eutectoid composition.**

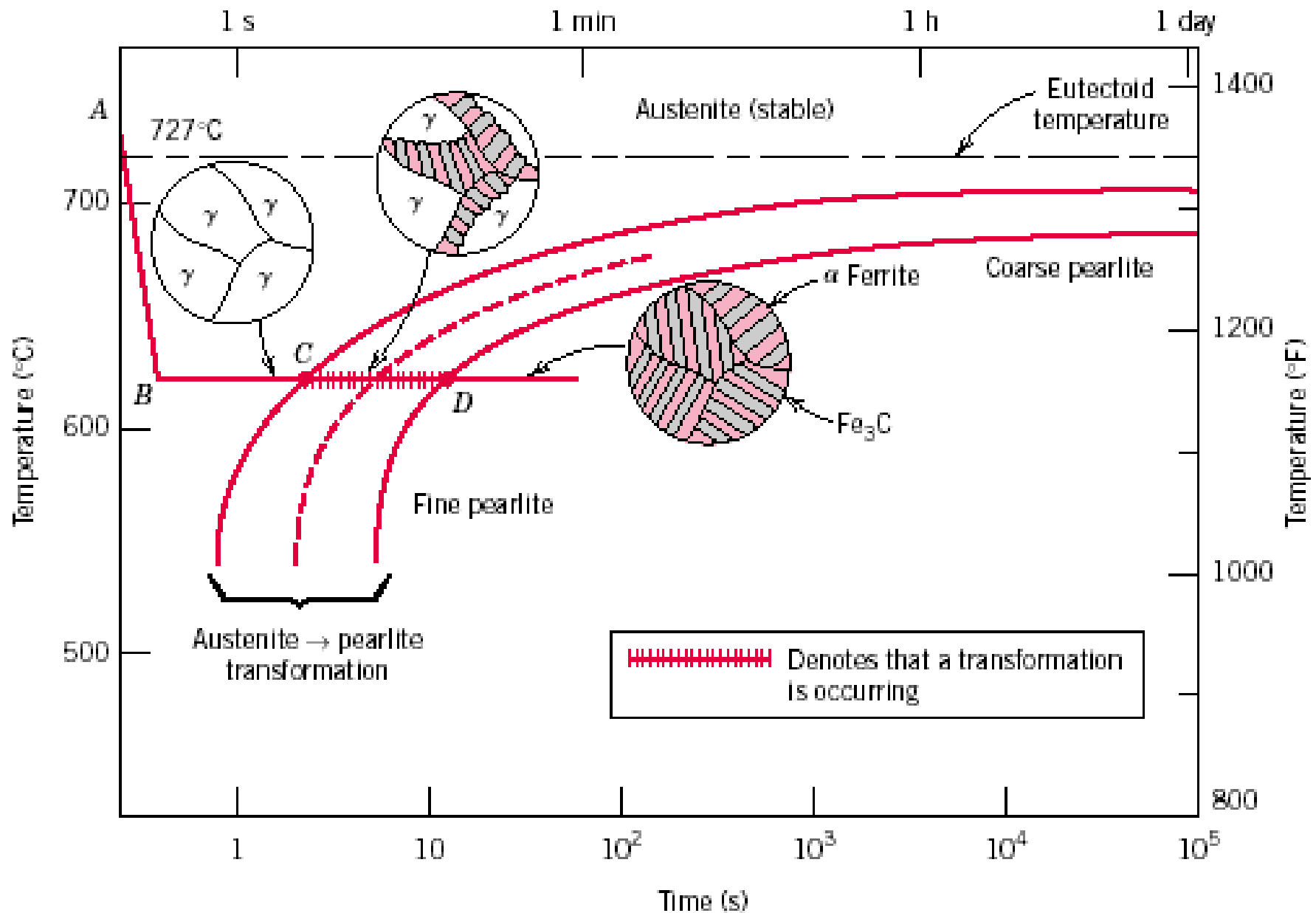
**A: austenite**

**B: bainite**

**M: martensite**

**P: pearlite**

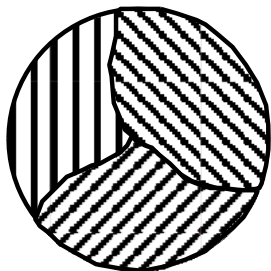
# TTT Diagram for a Eutectoid Fe-C Alloy



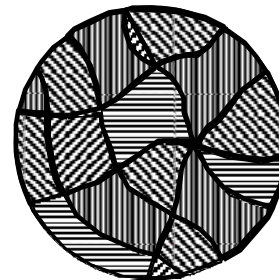
# Time-Temperature-Transformation (T-T-T) Diagrams

## Pearlite

- The thickness of the ferrite/cementite layers in pearlite depends on the temperature. With decreasing temperature, the layers become progressively thinner.
  - At temperatures just below eutectoid → relatively thick layers → coarse pearlite
  - In the vicinity of 540 °C → relatively thin layers → fine pearlite

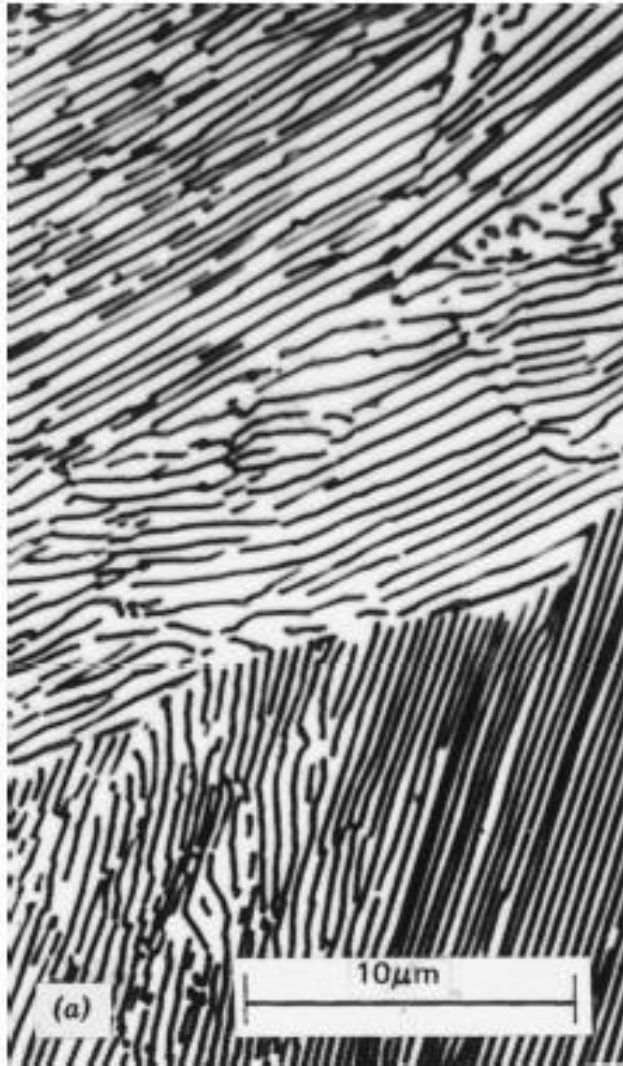


- Smaller  $\Delta T$ :  
colonies are  
larger

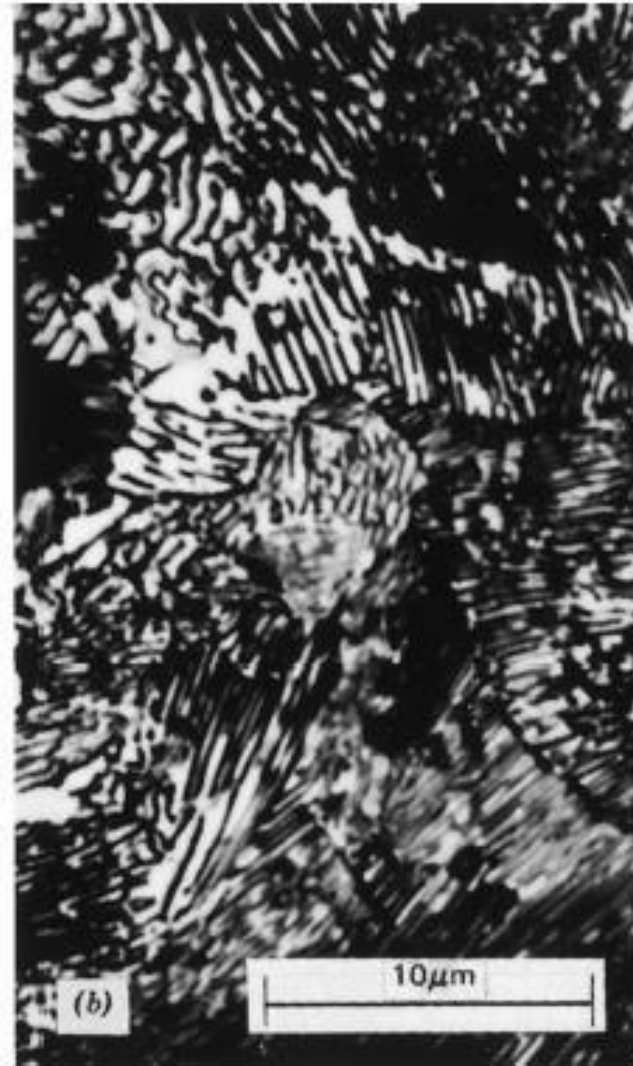


- Larger  $\Delta T$ :  
colonies are  
smaller



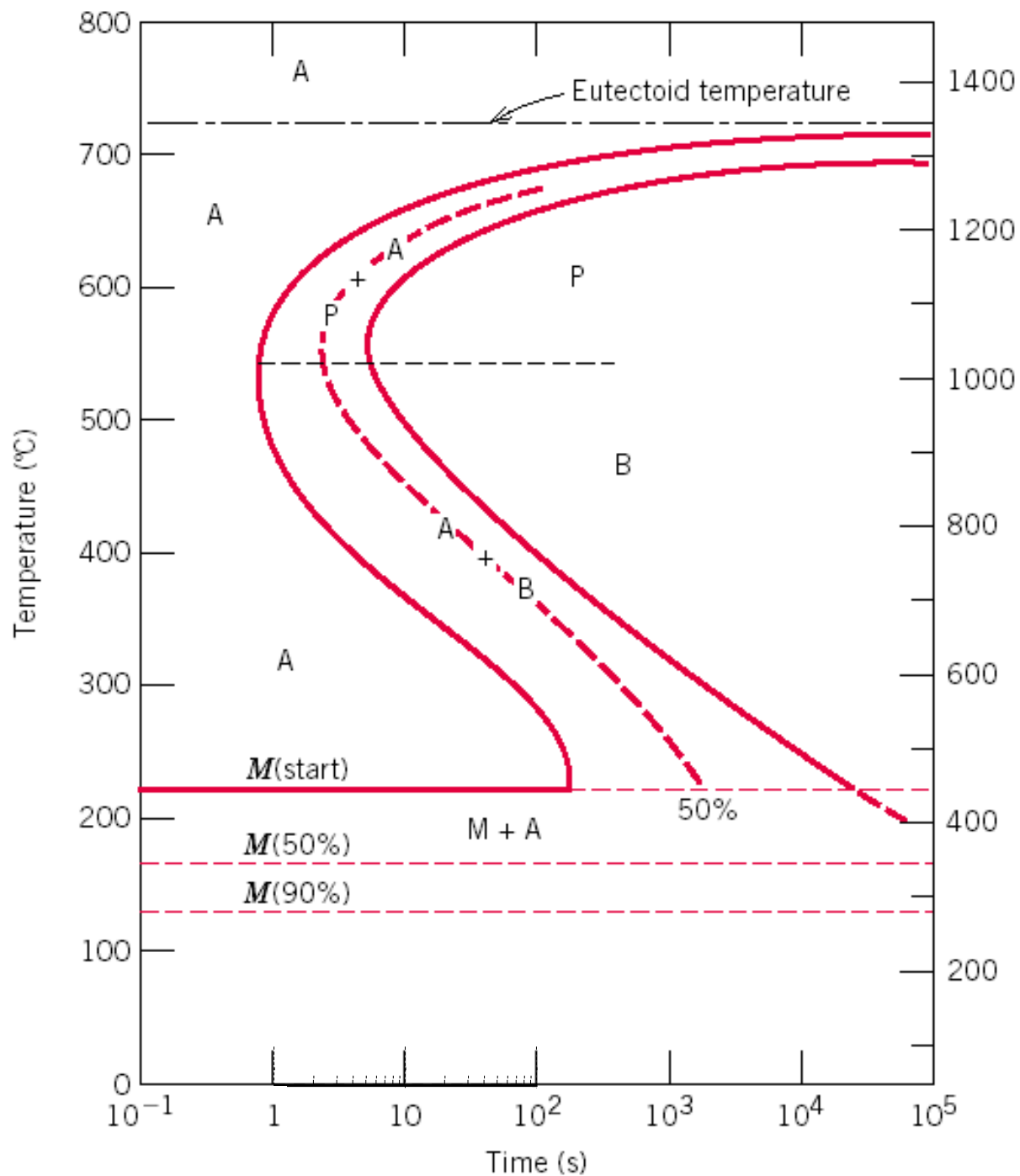


**(a) Coarse Pearlite**



**(b) Fine Pearlite**

**Photomicrographs of (a) coarse pearlite and (b) fine pearlite. 3000X.**



**The complete isothermal transformation diagram for an iron-carbon alloy of eutectoid composition.**

**A: austenite**

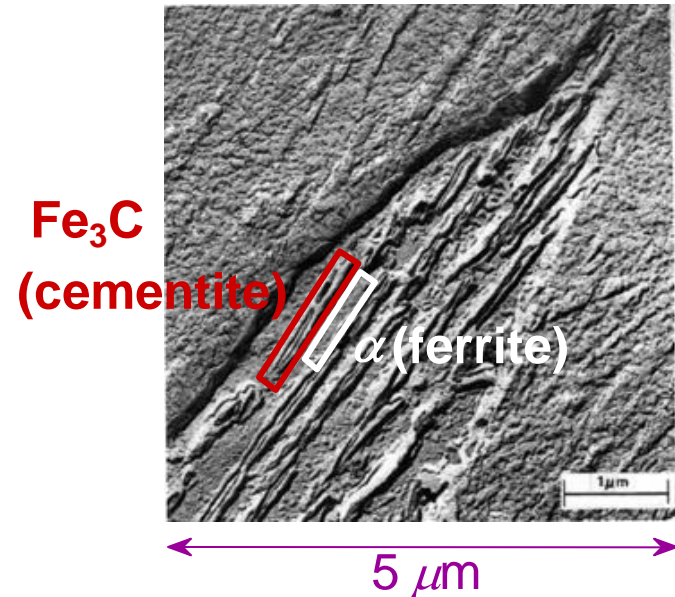
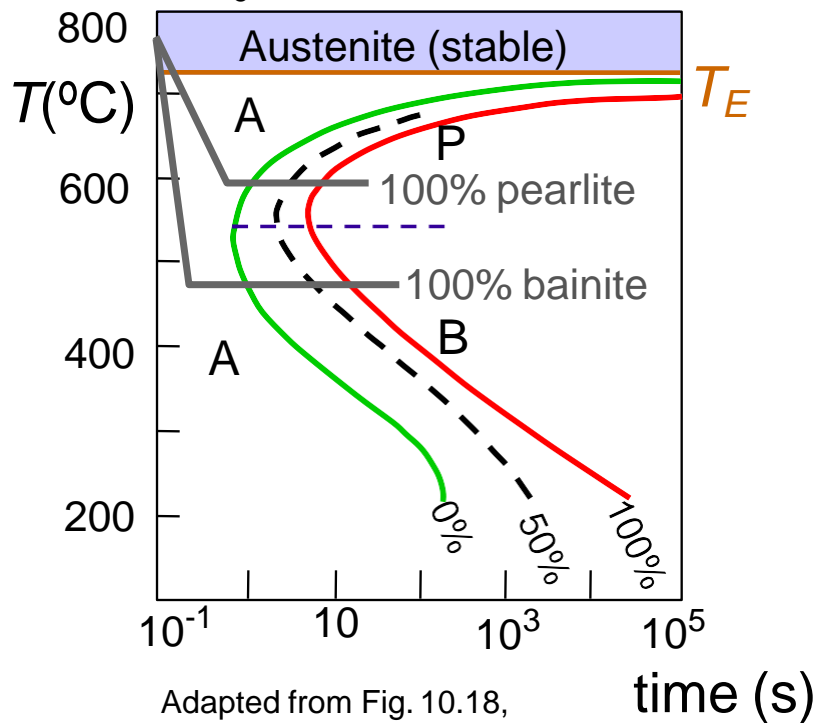
**B: bainite**

**M: martensite**

**P: pearlite**

# Bainite: Another Fe-Fe<sub>3</sub>C Transformation Product

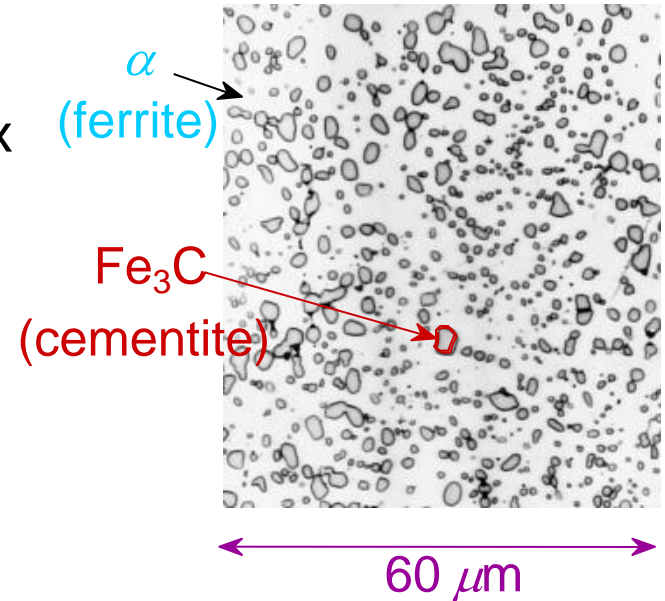
- Bainite:
  - elongated Fe<sub>3</sub>C particles in  $\alpha$ -ferrite matrix
  - diffusion controlled
- Isothermal Transf. Diagram,  $C_0 = 0.76 \text{ wt\% C}$



Adapted from Fig. 10.17, Callister & Rethwisch 8e. (Fig. 10.17 from *Metals Handbook*, 8th ed., Vol. 8, *Metallography, Structures, and Phase Diagrams*, American Society for Metals, Materials Park, OH, 1973.)

# Spheroidite: Another Microstructure for the Fe-Fe<sub>3</sub>C System

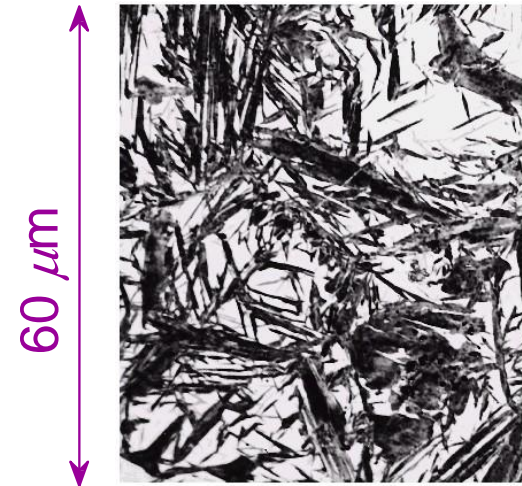
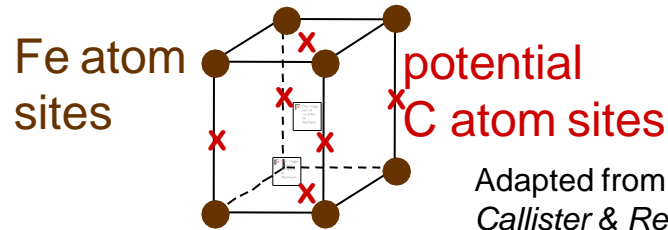
- **Spheroidite:**
  - Fe<sub>3</sub>C particles within an  $\alpha$ -ferrite matrix
  - formation requires diffusion
  - heat bainite or pearlite at temperature just below eutectoid for long times
  - driving force – reduction of  $\alpha$ -ferrite/Fe<sub>3</sub>C interfacial area



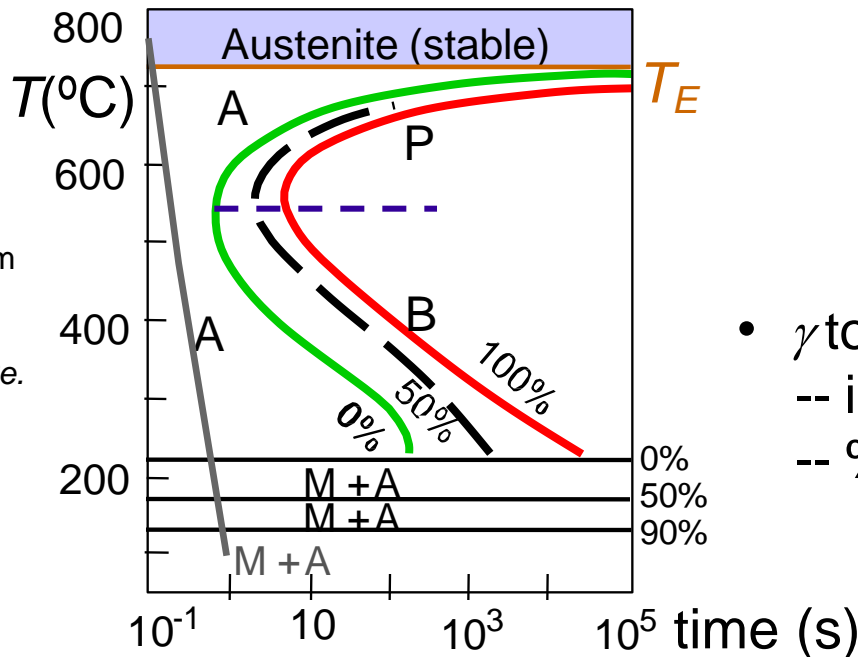
Adapted from Fig. 10.19, *Callister & Rethwisch 8e*. (Fig. 10.19 copyright United States Steel Corporation, 1971.)

# Martensite: A Nonequilibrium Transformation Product

- **Martensite:**  
 --  $\gamma$ (FCC) to Martensite (BCT)



- Isothermal Transf. Diagram

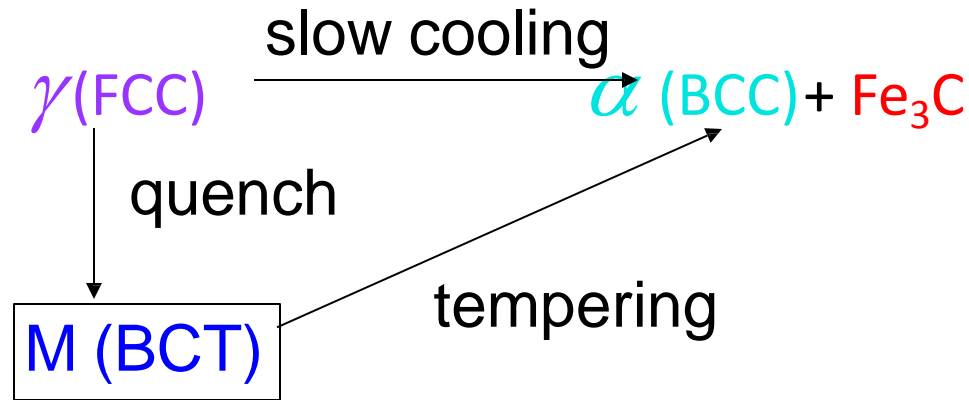


— Martensite needles  
 — Austenite

Adapted from Fig. 10.21, Callister & Rethwisch 8e. (Fig. 10.21 courtesy United States Steel Corporation.)

- $\gamma$  to martensite (M) transformation..  
 -- is rapid! (diffusionless)  
 -- % transf. depends only on  $T$  to which rapidly cooled

# Martensite Formation

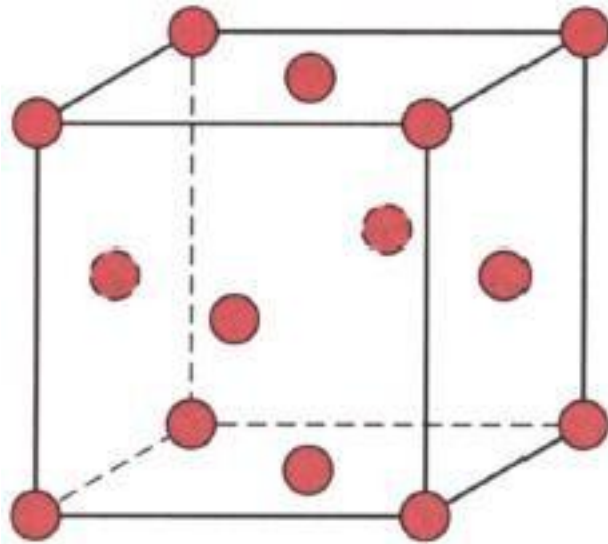


**Martensite (M)** – single phase  
– has body centered tetragonal (BCT)  
crystal structure

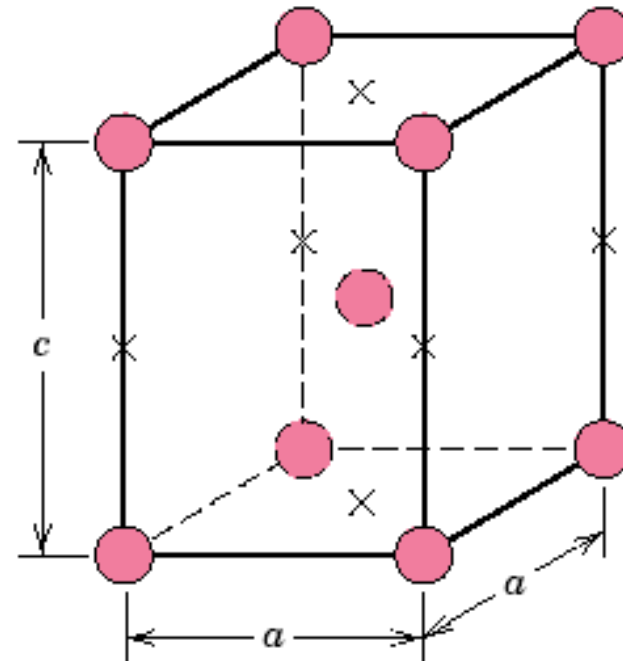
Diffusionless transformation      BCT if  $C_0 > 0.15$  wt% C  
BCT  $\rightarrow$  few slip planes  $\rightarrow$  hard, brittle

# Martensite

- Martensite is formed when austenitized Fe-C alloys are rapidly cooled (or quenched) to a relatively low temperature (in the vicinity of the ambient).
  - Non-equilibrium single phase
  - A transformation product that is competitive with pearlite
  - Transformation of FCC to BCT (body-centered tetragonal)
  - **Occurs instantaneously** → time-independent
  - The martensite grains nucleate and grow at a very rapid rate — the velocity of sound within the austenite matrix.



**FCC Austenite  
( $\gamma$  phase)**



**BCT Martensite  
(body-centered tetragonal)**

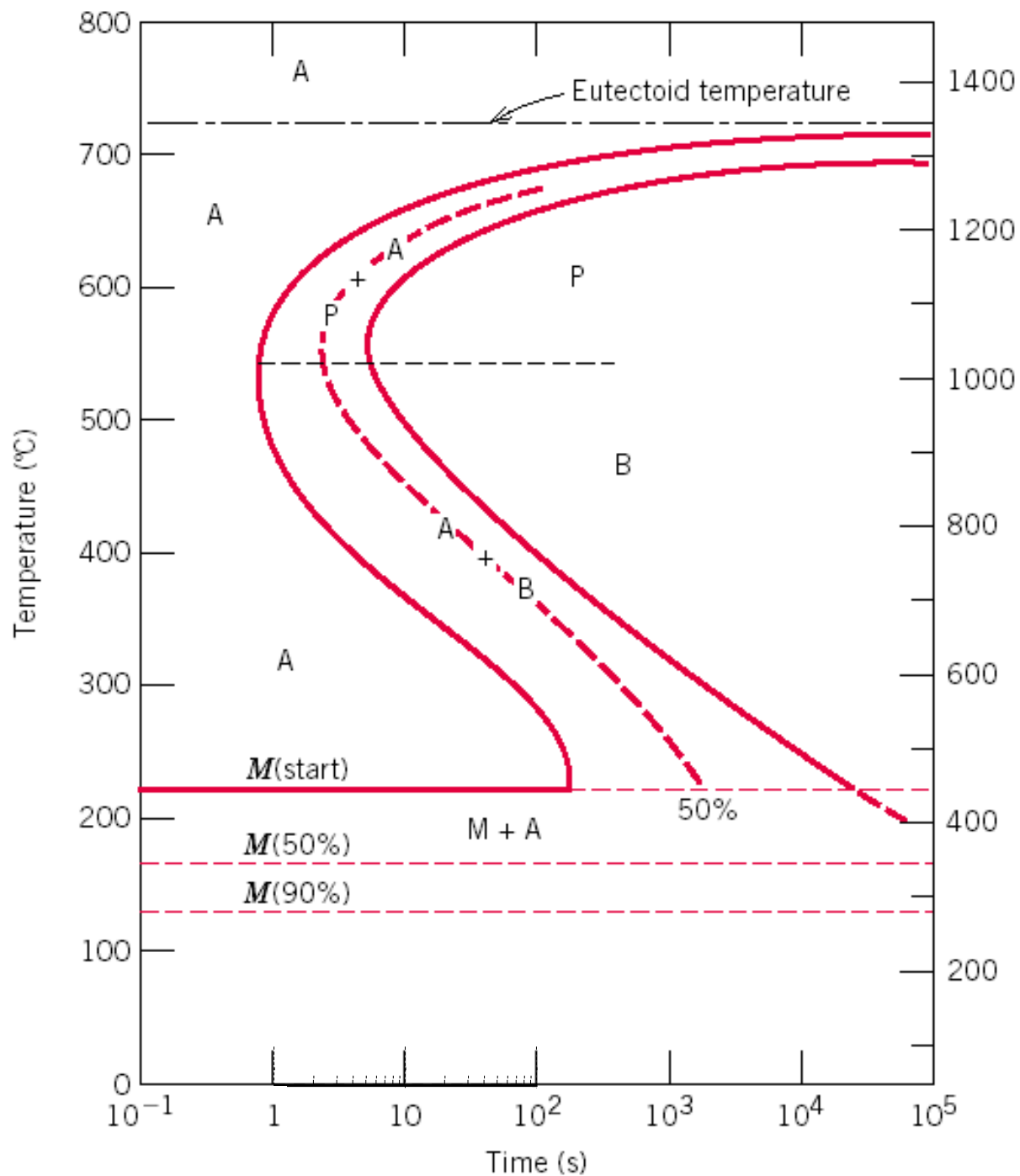
**The body-centered tetragonal unit cell for martensitic steel showing iron atoms (circles) and sites that may be occupied by carbon atoms (crosses). For this tetragonal unit cell,  $c > a$ .**





## **Lenticular or plate martensitic microstructure**

**Photomicrograph showing the lenticular or plate martensitic microstructure. The needle-shaped grains are the martensite phase, and the white regions are austenite that failed to transform during the rapid quench. 1220X.**



**The complete isothermal transformation diagram for an iron-carbon alloy of eutectoid composition.**

**A: austenite**

**B: bainite**

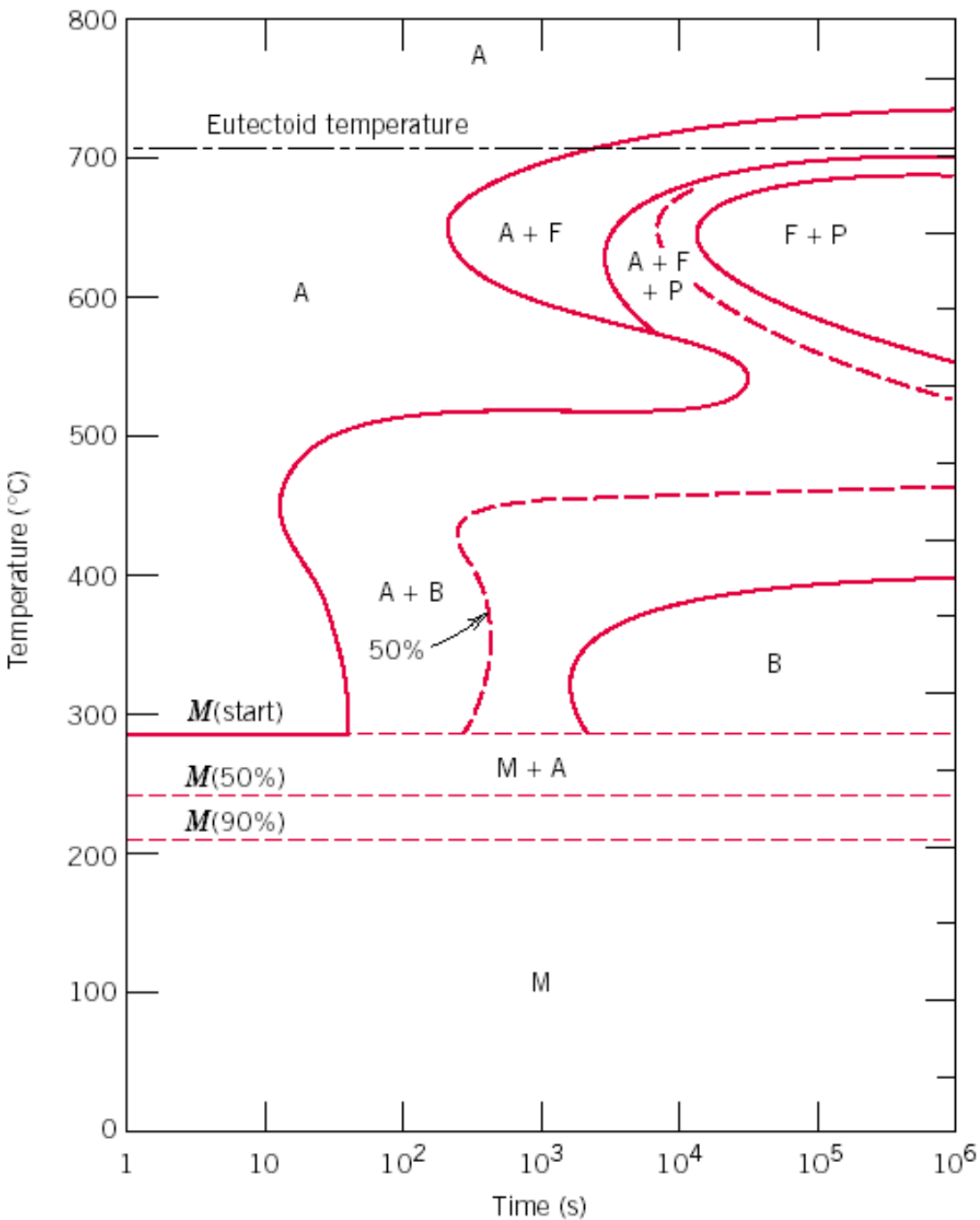
**M: martensite**

**P: pearlite**

# The Martensitic Transformation

Since the martensitic transformation is **instantaneous**, it is not depicted in this diagram like the pearlitic reaction.

- The beginning of this transformation is represented by a horizontal line designated M(start).
- Two other horizontal and dashed lines, labeled M(50%) and M(90%), indicate percentages of the austenite-to-martensite transformation.
- The temperatures at which these lines are located vary with alloy composition; **the temperatures must be relatively low.**
- **The horizontal and linear character of these lines indicates that the martensitic transformation is independent of time; it is a function only of the temperature to which the alloy is quenched.**



## Effects of alloying elements

The presence of alloying elements other than carbon (e.g., Cr, Ni, Mo, and W) may cause significant changes in the positions/shapes of the curves in the isothermal transformation diagrams.

**TTT diagram for an alloy steel (type 4340):**

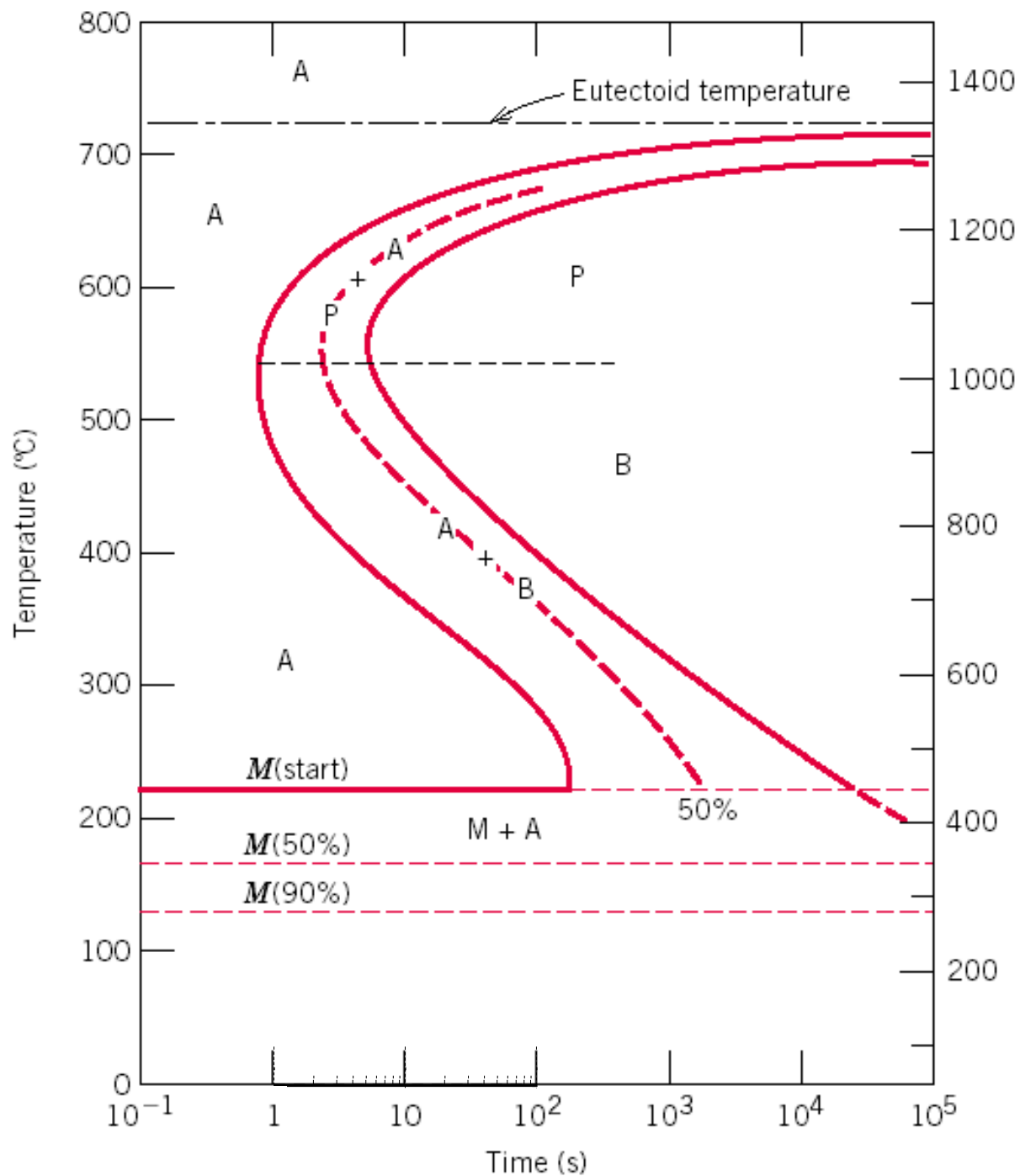
**A, austenite;**

**B, bainite;**

**P, pearlite;**

**M, martensite;**

**F, proeutectoid ferrite.**



**The complete isothermal transformation diagram for an iron-carbon alloy of eutectoid composition.**

**A: austenite**

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**M: martensite**

**P: pearlite**

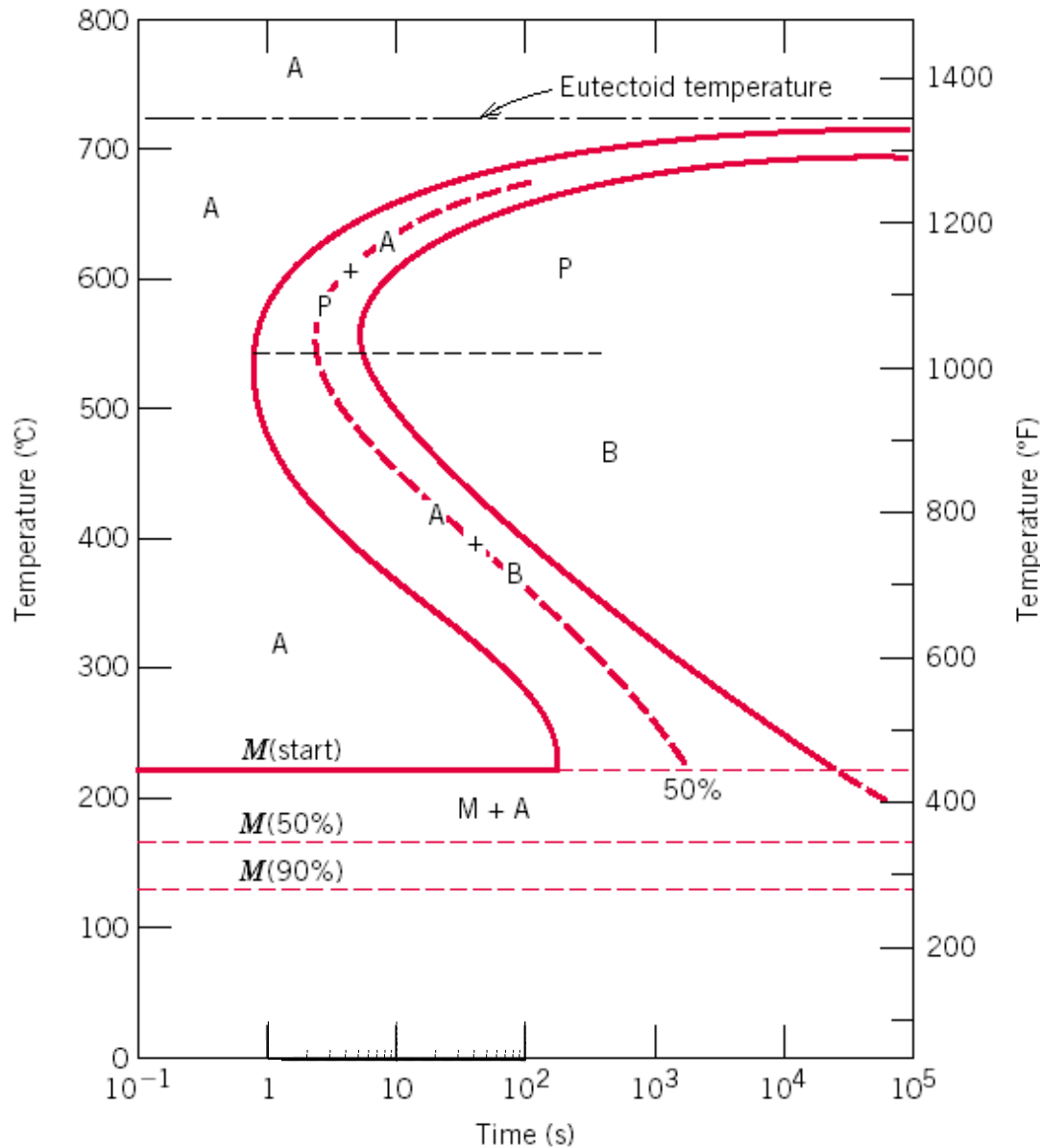
## Example Problem

Using the isothermal transformation diagram for an iron-carbon alloy of eutectoid composition, specify the nature of the final microstructure of a small specimen that has been subjected to the following time-temperature treatments.

The specimen begins at  $760^{\circ}\text{C}$  and that it has been held at this temperature long enough to have achieved a complete and homogeneous austenitic structure.

**(a) Rapidly cool to  $250^{\circ}\text{C}$ , hold for 100s, and quench to room temperature**

**(b) Rapidly cool to  $600^{\circ}\text{C}$ , hold for  $10^4\text{ s}$ , and quench to room temperature**

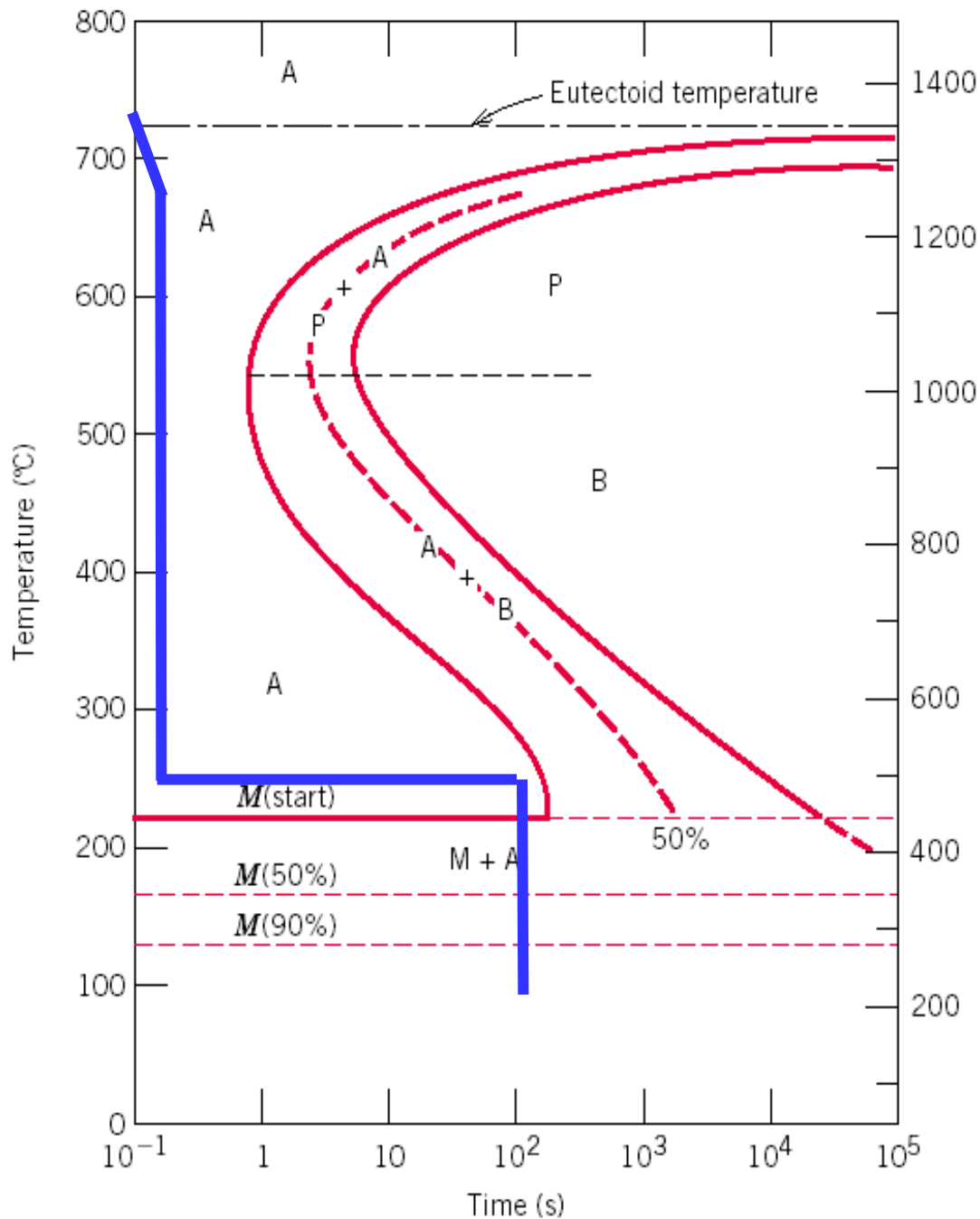


### Example Problem

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(b) Rapidly cool to  $600^{\circ}\text{C}$ , hold for  $10^4\text{ s}$ , and quench to room temperature

**The time-temperature-transformation diagram for an iron-carbon alloy of eutectoid composition and the isothermal heat treatments**

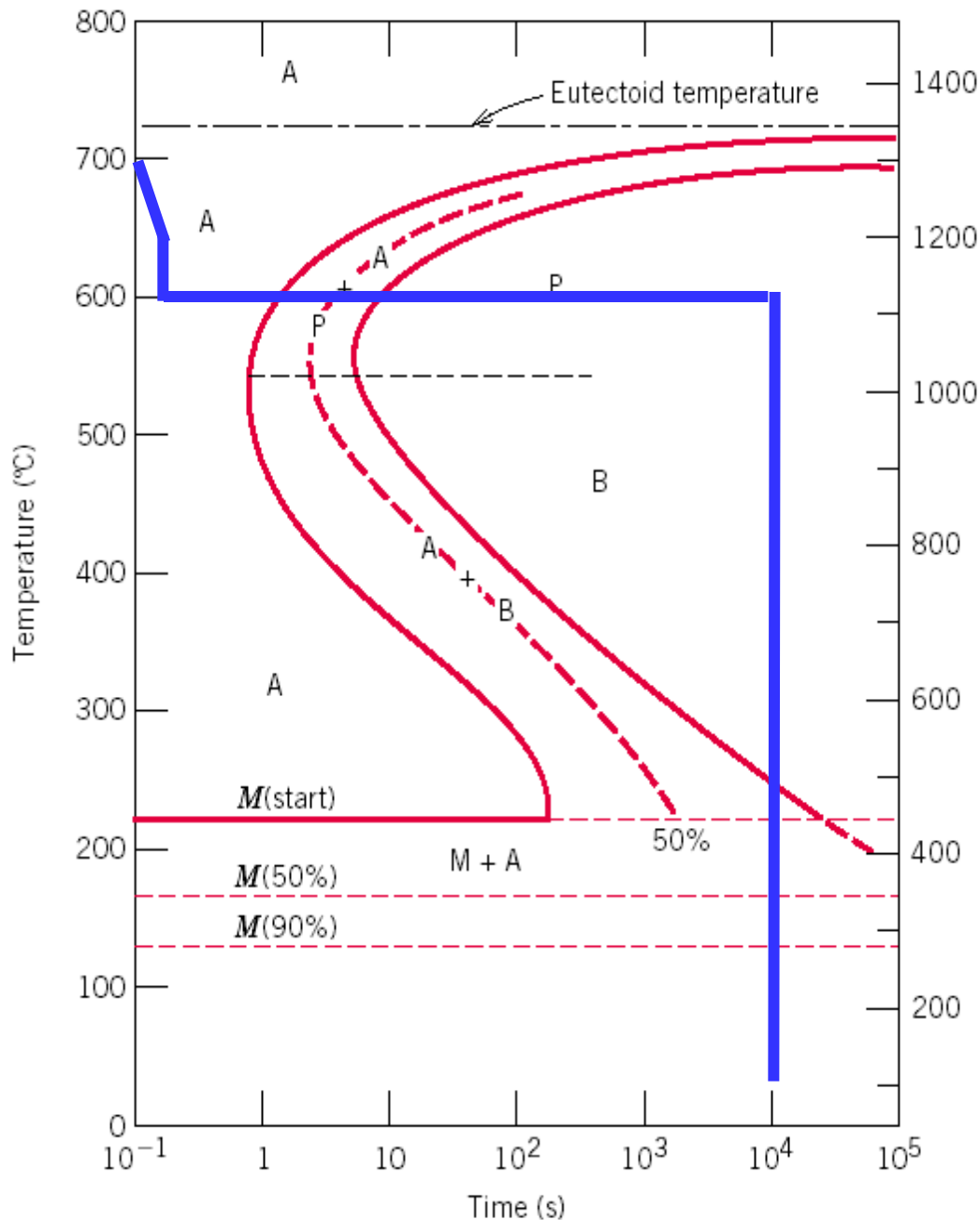


## Example Problem

**(a) Rapidly cool to 250° C, hold for 100s, and quench to room temperature**

- At 760° C: in the austenite region ( $\gamma$ )— 100% austenite
- Rapidly cool from 760° C to 250° C: 100% austenite
- Hold for 100 seconds at 250° C: 100% austenite
- Quench to room temp.: 100% martensite





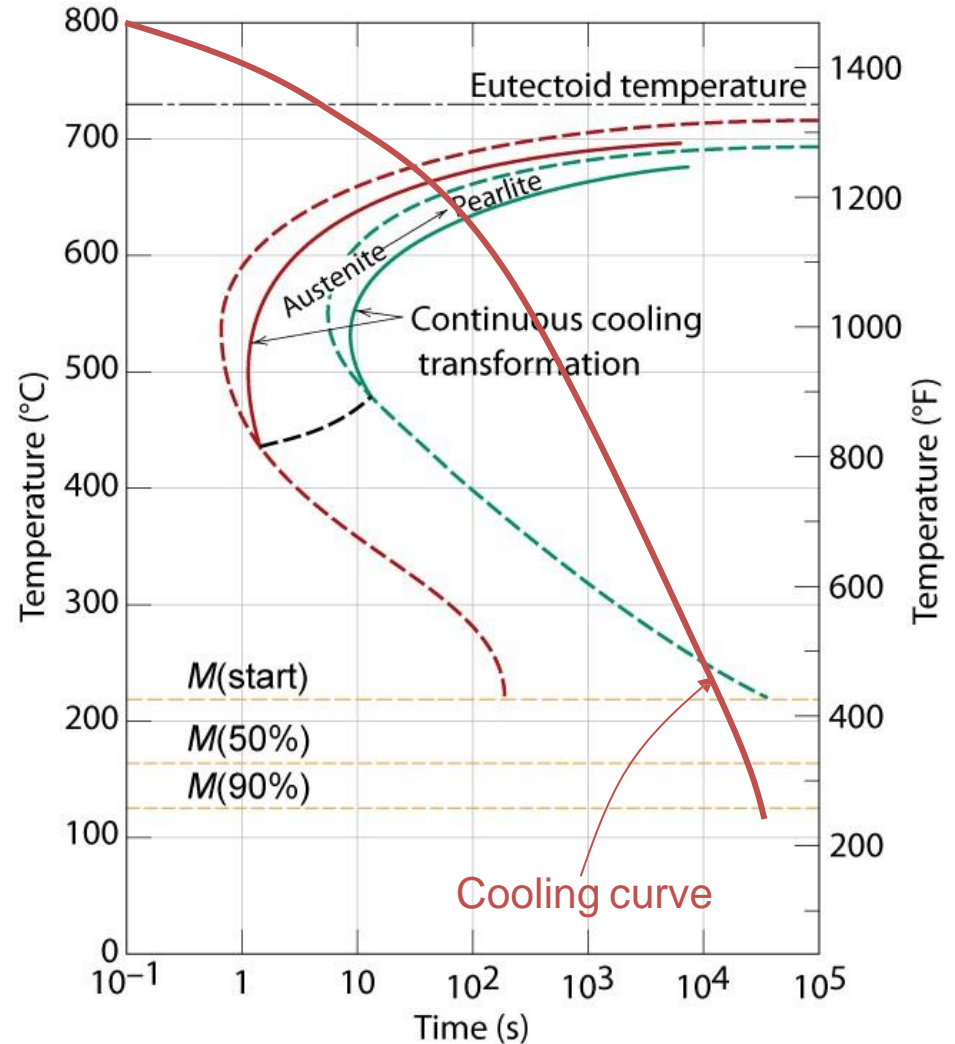
## Example Problem

**(b) Rapidly cool to 600° C, hold for 10<sup>4</sup> s, and cool to room temperature**

- At 760° C: in the austenite region ( $\gamma$ )— 100% austenite
- Rapidly cool from 760° C to 600° C: 100% austenite
- Hold for 10<sup>4</sup> s at 250° C: 100% pearlite
- Quench to room temp.: 100% pearlite

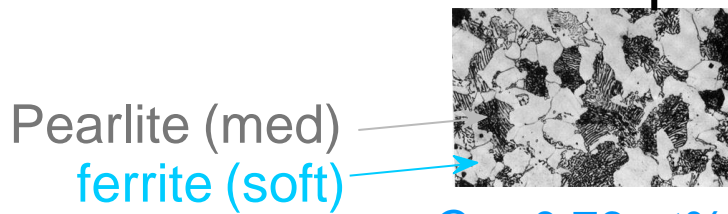
# Continuous Cooling Transformation Diagrams

Conversion of isothermal transformation diagram to continuous cooling transformation diagram



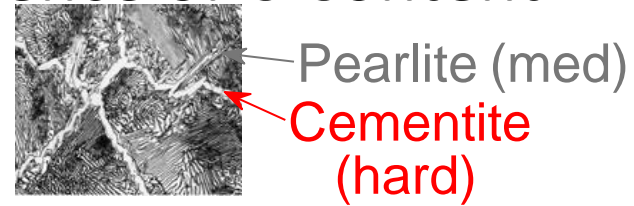
Adapted from Fig. 10.25,  
*Callister & Rethwisch 8e.*

# Mechanical Props: Influence of C Content



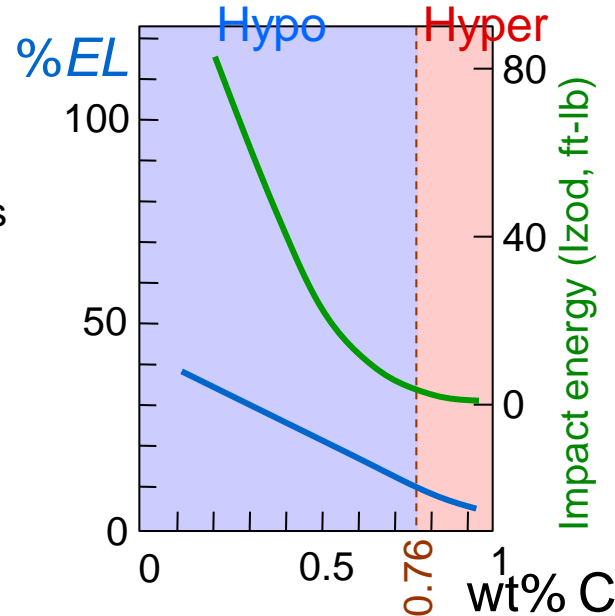
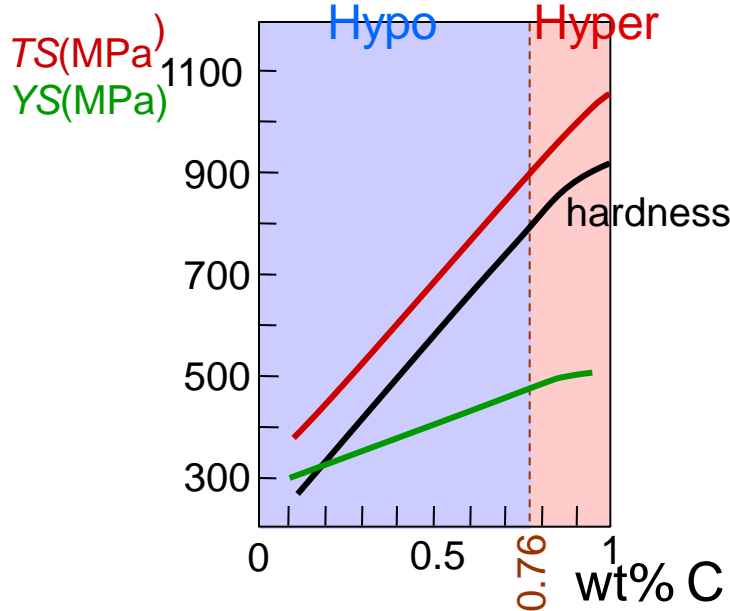
Adapted from Fig. 9.30,  
*Callister & Rethwisch 8e.*

$C_0 < 0.76 \text{ wt\% C}$   
Hypo



$C_0 > 0.76 \text{ wt\% C}$   
Hyper

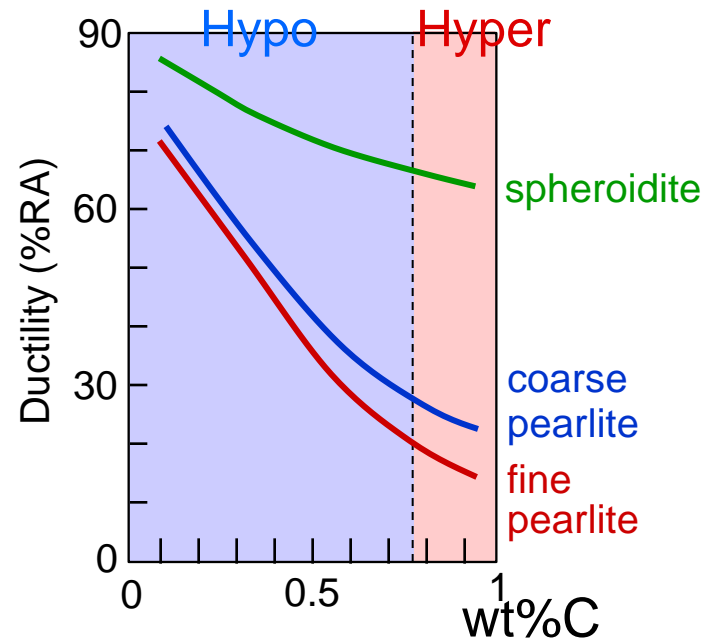
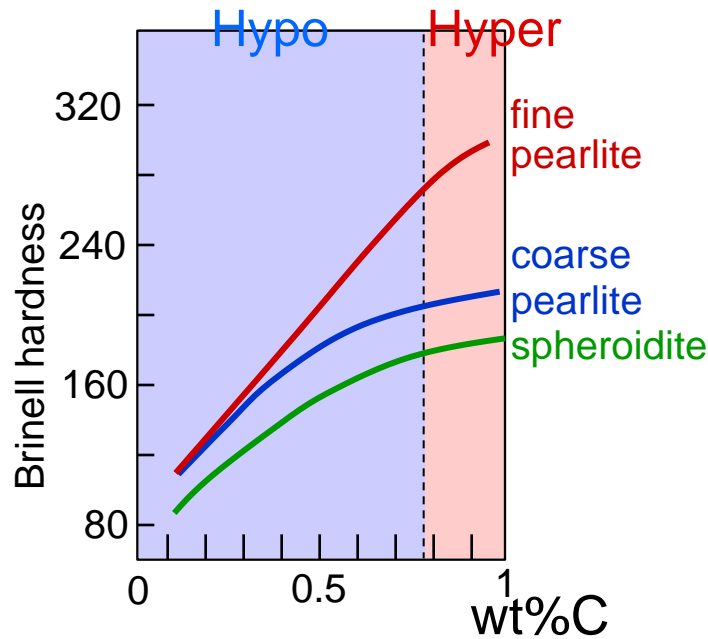
Adapted from Fig. 9.33,  
*Callister & Rethwisch 8e.*



Adapted from Fig. 10.29, *Callister & Rethwisch 8e.* (Fig. 10.29 based on data from *Metals Handbook: Heat Treating*, Vol. 4, 9th ed., V. Masseria (Managing Ed.), American Society for Metals, 1981, p. 9.)

- Increase C content:  $TS$  and  $YS$  increase,  $\%EL$  decreases

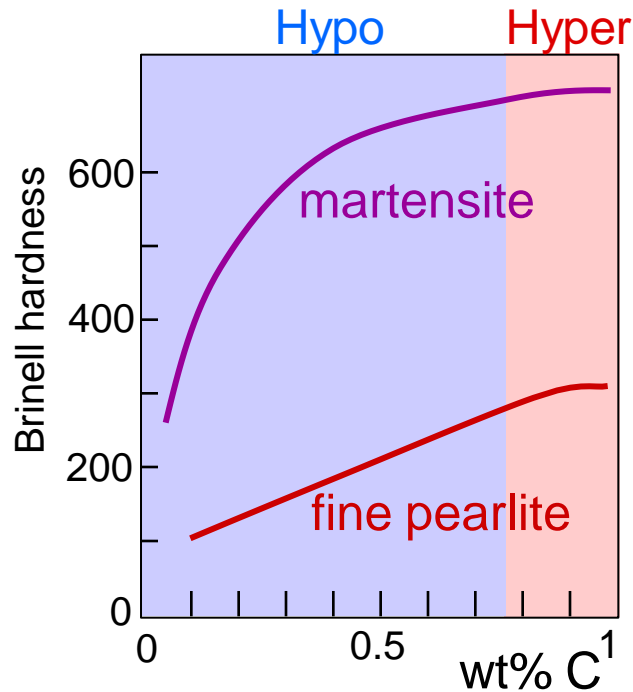
# Mechanical Props: Fine Pearlite vs. Coarse Pearlite vs. Spheroidite



- Hardness: fine > coarse > spheroidite
- %RA: fine < coarse < spheroidite

Adapted from Fig. 10.30, *Callister & Rethwisch 8e*. (Fig. 10.30 based on data from *Metals Handbook: Heat Treating*, Vol. 4, 9th ed., V. Masseria (Managing Ed.), American Society for Metals, 1981, pp. 9 and 17.)

# Mechanical Props: Fine Pearlite vs. Martensite



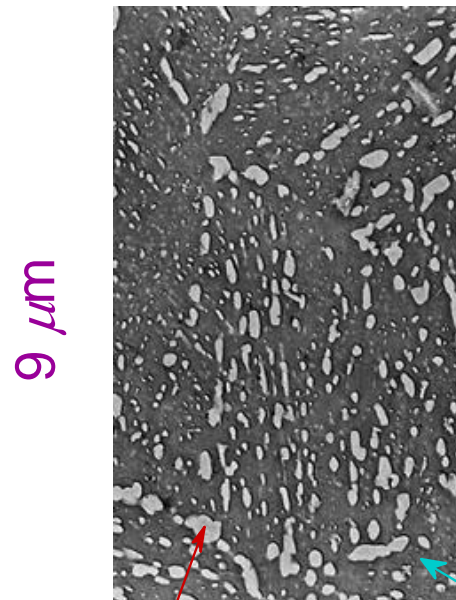
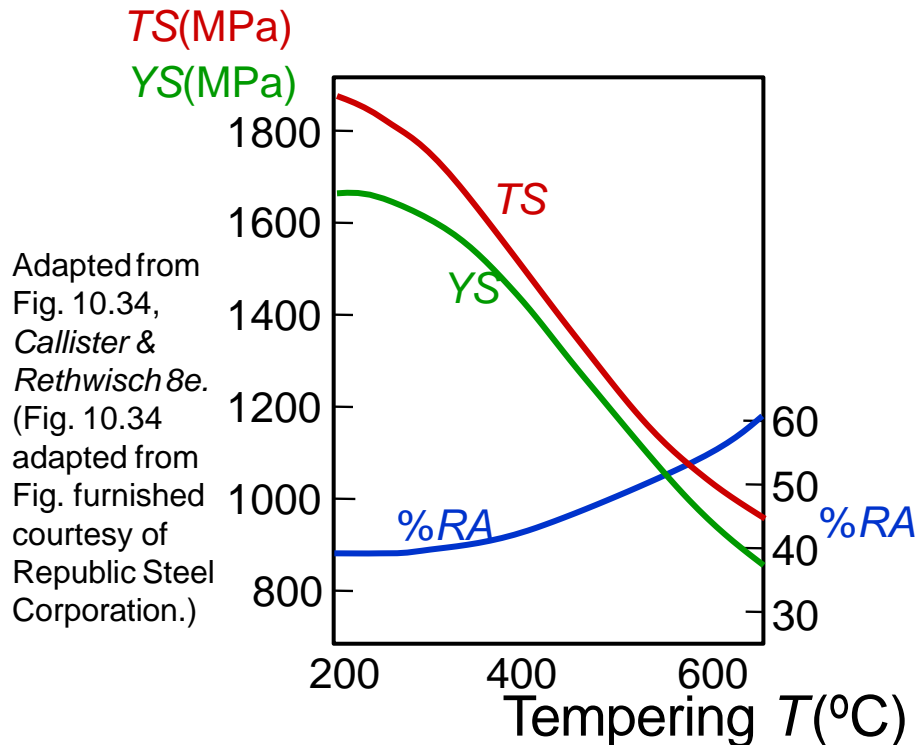
Adapted from Fig. 10.32, *Callister & Rethwisch 8e*. (Fig. 10.32 adapted from Edgar C. Bain, *Functions of the Alloying Elements in Steel*, American Society for Metals, 1939, p. 36; and R.A. Grange, C.R. Hribal, and L.F. Porter, *Metall. Trans. A*, Vol. 8A, p. 1776.)

- Hardness: fine pearlite  $\ll$  martensite.

# Tempered Martensite

Heat treat martensite to form tempered martensite

- tempered martensite less brittle than martensite
- tempering reduces internal stresses caused by quenching

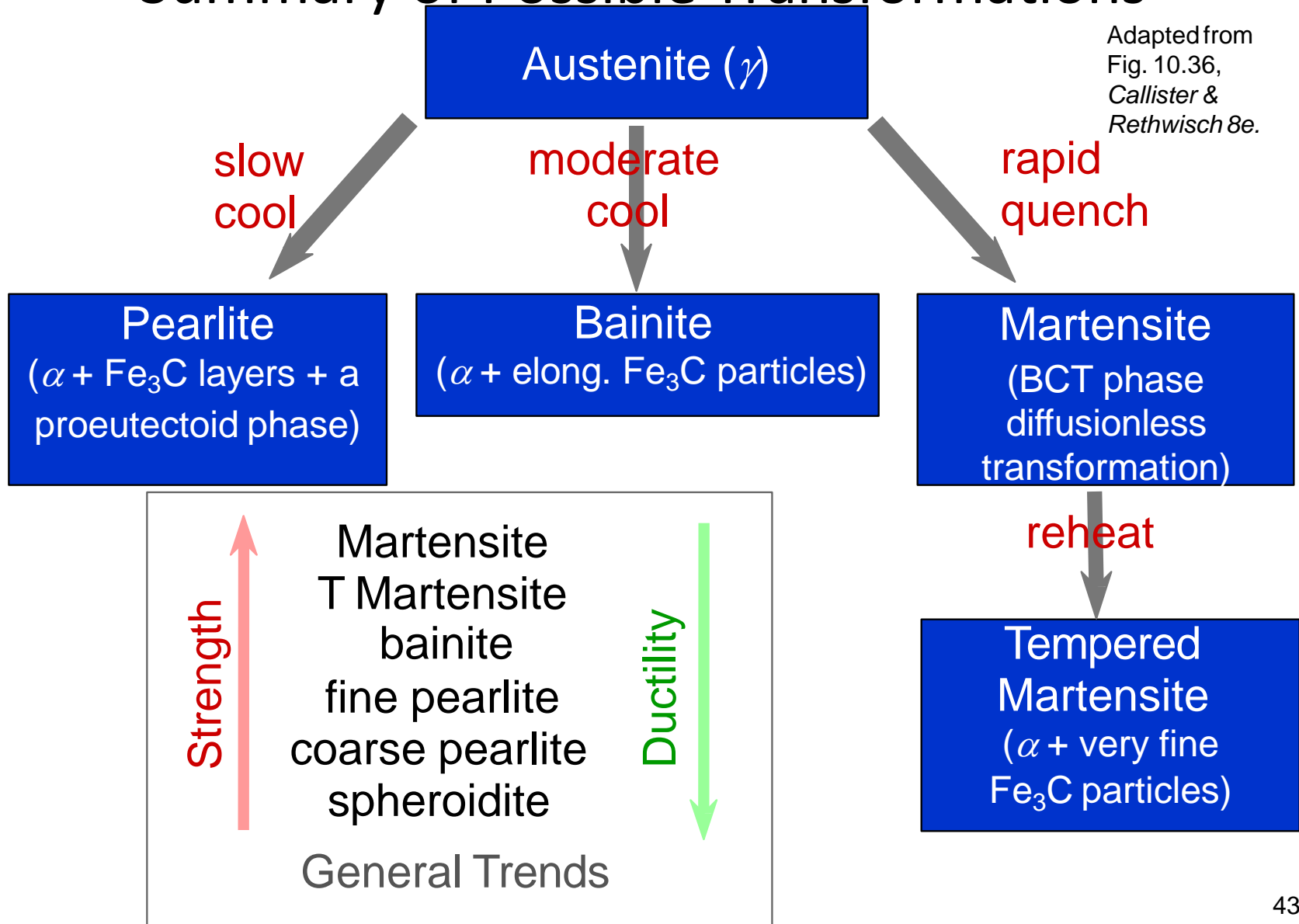


Adapted from Fig. 10.33, Callister & Rethwisch 8e. (Fig. 10.33 copyright by United States Steel Corporation, 1971.)

- tempering produces extremely small  $\text{Fe}_3\text{C}$  particles surrounded by  $\alpha$ .
- tempering decreases  $TS$ ,  $YS$  but increases  $\%RA$

# Summary of Possible Transformations

Adapted from  
Fig. 10.36,  
Callister &  
Rethwisch 8e.



**Table 10.2** Summary of Microstructures and Mechanical Properties for Iron–Carbon Alloys

<i>Microconstituent</i>	<i>Phases Present</i>	<i>Arrangement of Phases</i>	<i>Mechanical Properties (Relative)</i>
Spheroidite	$\alpha$ Ferrite + $\text{Fe}_3\text{C}$	Relatively small $\text{Fe}_3\text{C}$ sphere-like particles in an $\alpha$ -ferrite matrix	Soft and ductile
Coarse pearlite	$\alpha$ Ferrite + $\text{Fe}_3\text{C}$	Alternating layers of $\alpha$ ferrite and $\text{Fe}_3\text{C}$ that are relatively thick	Harder and stronger than spheroidite, but not as ductile as spheroidite
Fine pearlite	$\alpha$ Ferrite + $\text{Fe}_3\text{C}$	Alternating layers of $\alpha$ ferrite and $\text{Fe}_3\text{C}$ that are relatively thin	Harder and stronger than coarse pearlite, but not as ductile as coarse pearlite
Bainite	$\alpha$ Ferrite + $\text{Fe}_3\text{C}$	Very fine and elongated particles of $\text{Fe}_3\text{C}$ in an $\alpha$ -ferrite matrix	Hardness and strength greater than fine pearlite; hardness less than martensite; ductility greater than martensite
Tempered martensite	$\alpha$ Ferrite + $\text{Fe}_3\text{C}$	Very small $\text{Fe}_3\text{C}$ sphere-like particles in an $\alpha$ -ferrite matrix	Strong; not as hard as martensite, but much more ductile than martensite
Martensite	Body-centered tetragonal, single phase	Needle-shaped grains	Very hard and very brittle

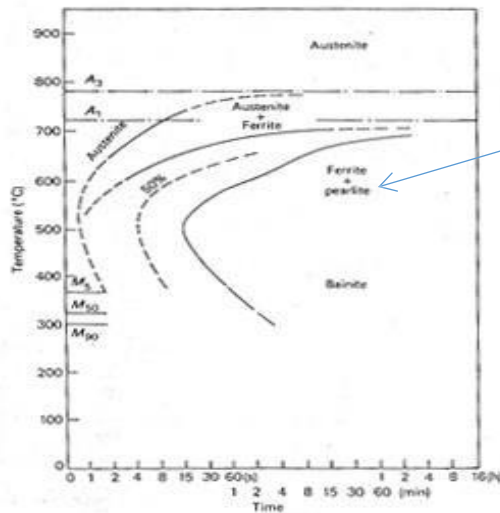


# Hardenability

- We have seen the advantage of getting martensite, M. We can temper it, getting TM with the best combination of ductility and strength.
- But the problem is this: getting M in depth, instead of just on the surface. We want a steel where Pearlite formation is relatively sluggish so we can get it to the cooler regions where M forms.
- The ability to get M (martensite) in depth for low cooling rates is called hardenability.
- Plain carbon steels have poor hardenability.

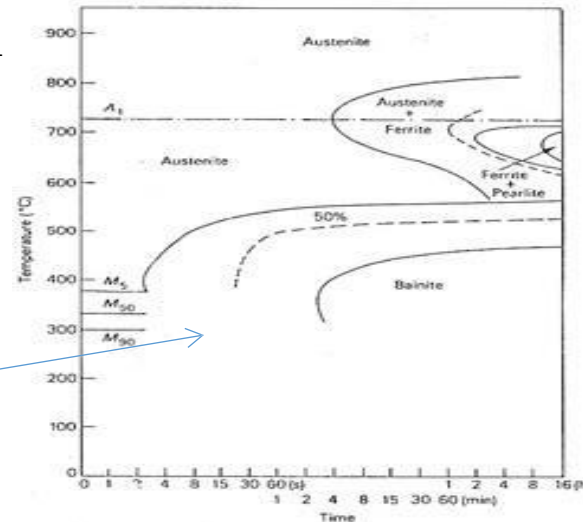
# Factors Which Improve Hardenability

- 1. Austenitic Grain size. The Pearlite will have an easier time forming if there is a lot of g.b. area. Hence, having a large austenitic grain size improves hardenability.
- 2. Adding alloys of various kinds. This impedes the  $\gamma \rightarrow P$  reaction.



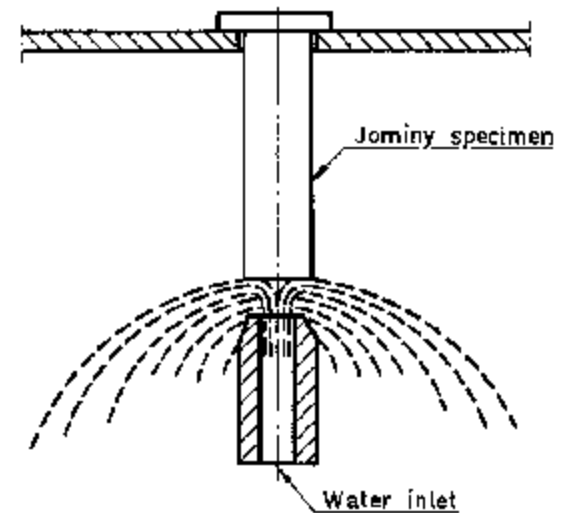
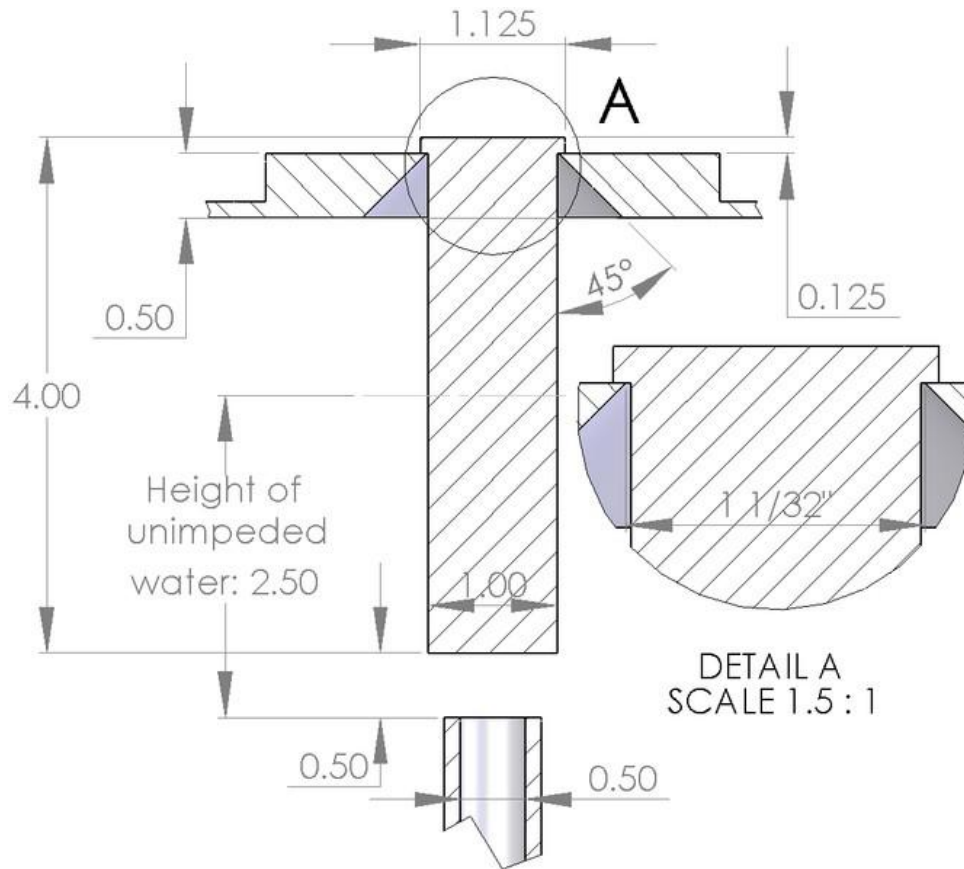
TTT diagram  
of a  
molybdenum  
steel 0.4C  
0.2Mo

After  
Adding  
2.0% Mo

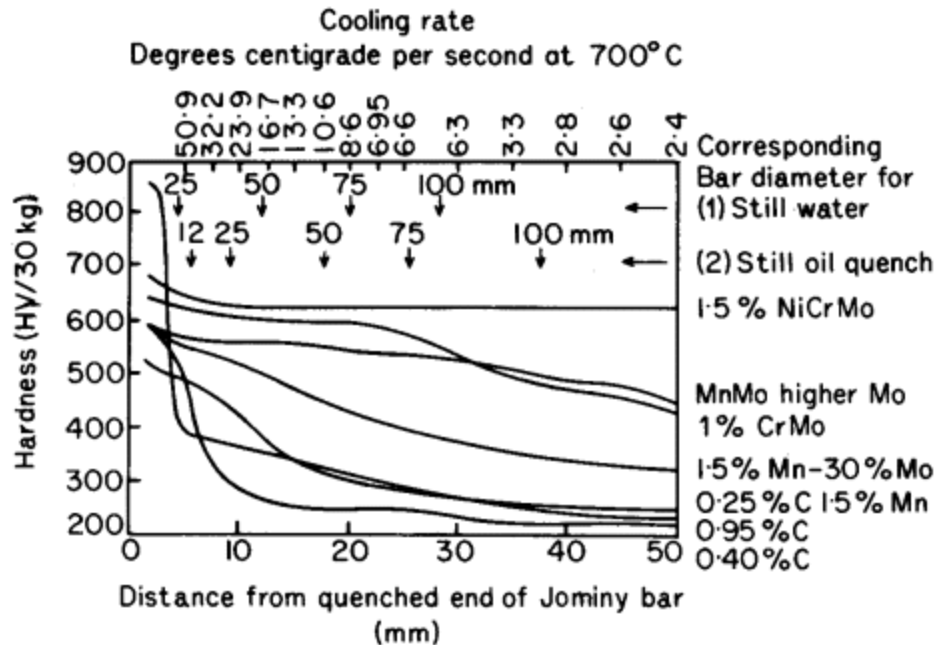


# Jominy Test for Hardenability

- Hardenability not the same as hardness!



# The Result is Presented in a Curve

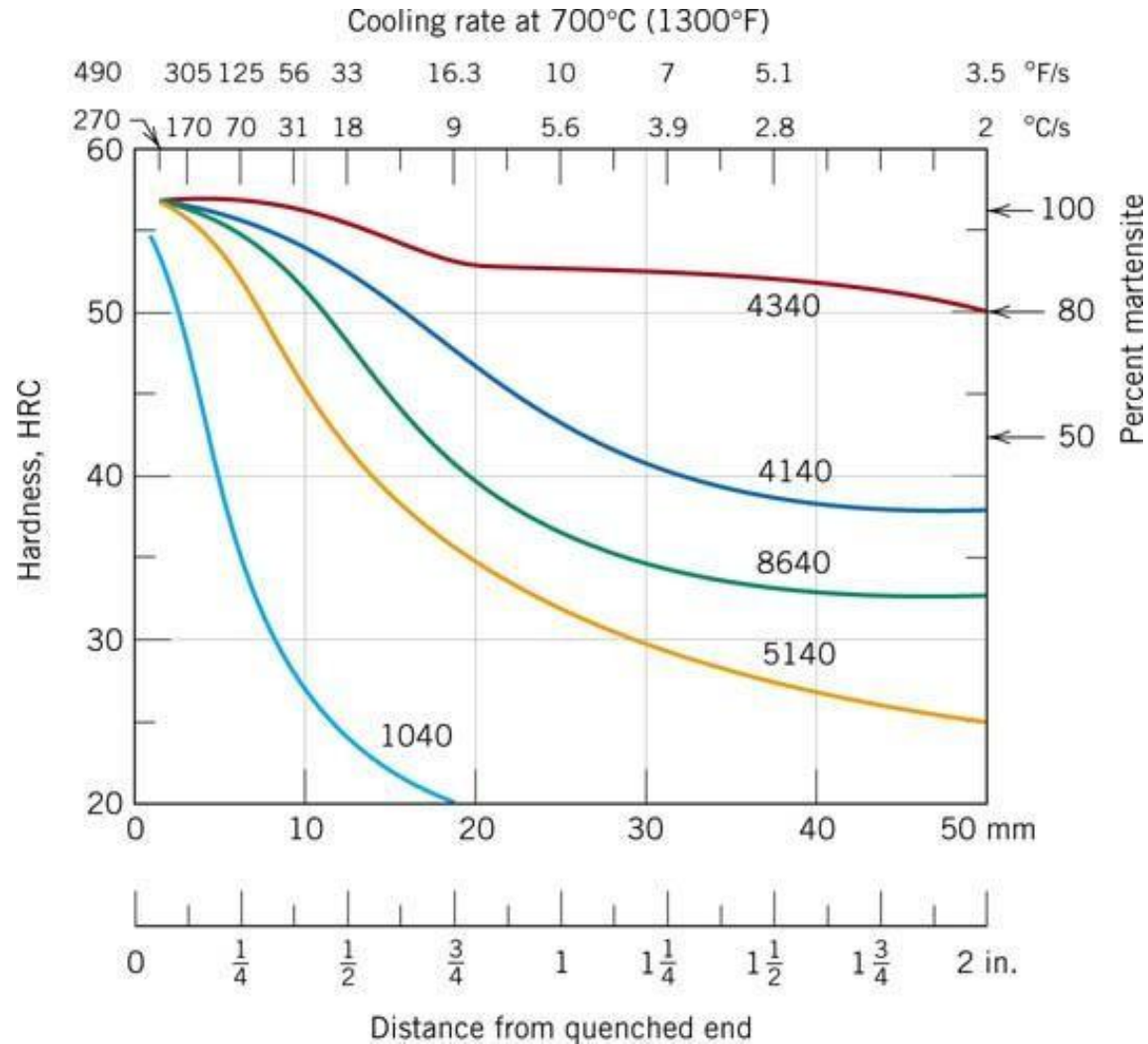


Note:

1. Distance from quenched end corresponds to a cooling rate, and a bar diameter
2. Notice that some steels drop off more than others at low cooling rates. Less hardenability!

Rank steels in order of hardenability.

# Alloying and Hardenability



# Carbon and Hardenability

